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Commissioner for Patents
Washington, D.C. 20231

PCT/JP00/06271
-filed September 13, 2000

Re: Application of Hideaki IURA, Youichi YAMAMOTO, and
Tomohiro KAWACHI
CONTROL METHOD OF AC MOTOR AND CONTROL APPARATUS
THEREOF
Assignee: **KABUSHIKI KAISHA YASKAWA DENKI**
Our Ref: Q69003

Dear Sir:

The following documents and fees are submitted herewith in connection with the above application for the purpose of entering the National stage under 35 U.S.C. § 371 and in accordance with Chapter II of the Patent Cooperation Treaty:

- ☒ an executed Declaration and Power of Attorney.
- ☒ an English translation of the International Application.
- ☒ twelve (12) sheets of drawings.
- ☒ an executed Assignment and PTO 1595 form.
- ☒ Notification Concerning Submission or Transmittal of Priority Document.
- ☒ a Form PTO-1449 listing the ISR references, and a complete copy of each reference.
- ☒ a Preliminary Amendment

It is assumed that copies of the International Application, the International Search Report, the International Preliminary Examination Report, and any Articles 19 and 34 amendments as required by § 371(c) will be supplied directly by the International Bureau, but if further copies are needed, the undersigned can easily provide them upon request.

The Government filing fee is calculated as follows:

Total claims	33	-	20	=	13	x	\$18.00	=	\$234.00
Independent claims	4	-	3	=	1	x	\$84.00	=	\$84.00
Base Fee									\$890.00
Multiple Dependent Claim Fee									\$280.00
TOTAL FILING FEE									\$1488.00
Recordation of Assignment									\$ 40.00
TOTAL FEE									\$1528.00

Checks for the statutory filing fee of \$1488.00 and Assignment recordation fee of \$40.00 are attached. You are also directed and authorized to charge or credit any difference or



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National Stage Entry of PCT/JP00/06271
Q69003

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overpayment to Deposit Account No. 19-4880. The Commissioner is hereby authorized to charge any fees under 37 C.F.R. §§ 1.16, 1.17 and 1.492 which may be required during the entire pendency of the application to Deposit Account No. 19-4880. A duplicate copy of this transmittal letter is attached.

Priority is claimed from:

<u>Country</u>	<u>Application No</u>	<u>Filing Date</u>
Japan	11-267499	September 21, 1999
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Respectfully submitted,

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PATENT APPLICATION

In re application of

Hideaki IURA, et al.

Appln. No.: National Stage of PCT/JP00/06271

Confirmation No.: NOT YET ASSIGNED

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For: CONTROL METHOD OF AC MOTOR AND CONTROL APPARATUS THEREOF

PRELIMINARY AMENDMENT

Commissioner for Patents
Washington, D.C. 20231

Sir:

Prior to examination, please amend the above-identified application as follows:

IN THE SPECIFICATION:

Page 14, Please delete the sixth full paragraph and replace with following new paragraph.

Fig. 6(a) and 6(b) are diagrams showing the relationship between the locus of the residual voltage of the AC motor and the output voltage command and phase (at the time of normal rotation) of a current controller.

Page 14, Please delete the seventh full paragraph and replace with following new paragraph.

Fig. 7(a) and 7(b) are diagrams showing the relationship between the locus of the residual voltage of the AC motor and the output voltage command and phase (at the time of reverse rotation) of the current controller.

12/pct/1

[Designation of Document]

Specification

[Title of the Invention]

Control method of AC motor and Control apparatus thereof

[Technical Field]

5 The present invention relates to a control method of an AC motor by which a speed of the AC motor is varied by a variable speed control apparatus to output the AC voltage, and specially to a control method and an apparatus by which the AC motor can be smoothly started after the return from the power failure.

10

[Background technology]

Conventionally, to speed control the AC motor, a V/f constant control method by which a ratio of the output voltage V and an output frequency f is made constant, is well known.

15 Further, recently, in order to more accurately control the AC motor, a vector control to respectively independently control the primary current to be supplied to the AC motor, in the exciting current (current to generate the magnetic flux) and the torque current (current to generate the torque) which

20 directly relate to the torque, is brought into the practical use. However, in the conventional control system, during the continuous running, the stable control is conducted, however, in the case where the instantaneous power failure is generated in the running of the AC motor once, and restarting after the

25 instantaneous power failure is conducted, when the residual voltage of the AC motor and the phase of the voltage command of the variable speed control apparatus are not matched, the

speed of the AC motor is rapidly changed, or a slip of the AC motor is increased, thereby, the over current flows, resulting in a danger such as a trip. In order to prevent this, it is necessary that the residual voltage of the AC motor and the phase of the voltage command of the variable speed control apparatus are matched, and the re-running is conducted, however, the matching of the phase is very difficult. Therefore, because, after the residual voltage does not exist, the angular velocity of the AC motor and the output frequency of the variable speed control apparatus are calculated from the speed detector, or the residual voltage of the AC motor is detected by the voltage detector, and by being calculated from its frequency component, the phases of the residual voltage and the output voltage command signal are made to coincide with each other, and re-running is conducted, there is a problem that the restart after the instantaneous power failure takes a long period of time, or a smooth re-running is difficult.

As described above, in order to smoothly start the AC motor, there is a problem that it is necessary to wait that the residual voltage does not exist, or the detector such as the speed detector or voltage detector is necessary.

Accordingly, the object of the present invention is to provide the control method and control apparatus of the AC motor by which, by accurately measuring the phase and angular velocity of the residual voltage of the AC motor after the recovery of the instantaneous power failure, the re-running can be quickly and smoothly conducted.

Disclosure of the Invention

The summary of a control method and control apparatus of the AC motor of the present invention to solve the above
5 problem, exists in the following (1) to (23).

(1) A control method of an AC motor which is characterized in that: it has an electric power converter to output the electric power to the AC motor, and is provided with a current control section to control the output current of the electric power converter based on the difference signal of the current
10 command signal and the output current detection signal of the electric power converter, and when the AC motor is in a free run condition, the current command signal is forcibly made zero so that the current of the AC motor is made zero, and current
15 controlled, and on the base of the output voltage command signal which is calculated by using the current control section output at this time, the amplitude and phase and angular velocity of the residual voltage of the AC motor are obtained.

(2) A control method of an AC motor according to (1), wherein,
20 when the phase and the angular velocity of the residual voltage of the AC motor are obtained based on the output voltage command signal, a signal holding means is provided, and the amplitude, and phase and angular velocity of the residual voltage are obtained from the addition value of the phase command signal
25 just before the AC motor free runs, and the phase signal of the output voltage command signal.

According to this control method of the AC motor, in the

case where the AC motor is in the free run condition, when it is controlled so that the current of the AC motor becomes zero, it is utilized as this result that the residual voltage of the AC motor appears in the voltage command signal, the amplitude and phase and angular velocity of the residual voltage of the AC motor which is in the free run condition, are obtained on the base of the phase and angular frequency of the this voltage command signal. Thereby, the smooth speed-return after the power failure recovery becomes easy.

Further, when the phase and angular velocity of the residual voltage are searched, a signal holding means is provided, and because the phase and angular velocity of the residual voltage are searched from the addition value of the phase command signal and the phase signal of the output voltage command signal just before the AC motor free-runs, there is no discontinuity of the phase command signal and a disadvantage such as the mechanical shock occurrence can be prevented.

(3) A control method of an AC motor which is characterized in that: in the control method by which an arbitrary electric power is outputted to the AC motor by the electric power converter, and the current supplied to the motor is detected by the current detection circuit, and it is controlled by the current control circuit so that the given current command and the current detection value detected by the current detection circuit coincide to each other, and the switching of the electric power converter is determined from the voltage command outputted from the current control circuit, the electric power

converter is controlled by a start control circuit so that it is normally operated at the start time, and the speed of the AC motor in the free run condition is estimated by a speed estimation circuit.

5 (4) A control method of an AC motor according to (3), wherein the start control circuit forcibly makes the current command zero, and by the current control circuit, the voltage command so that the current detection value is made zero, is calculated, and by the time change of the voltage command, the speed
10 estimation circuit estimates the speed of the AC motor.

(5) A control method of an AC motor according to either one of (3) or (4), wherein the start control circuit forcibly makes the current command zero, and by the current control circuit, the voltage command by which the current detection value is
15 made zero, is calculated, and when its voltage level is lower than the set voltage level, after the set level DC current command is applied for a set time period from zero, the current command is forcibly made zero again, and by the current control circuit, the voltage command by which the current detection
20 value is made zero, is calculated, and the speed estimation circuit estimates the speed of the AC motor.

(6) A control method of an AC motor according to any one of (3) to (5), wherein the start control circuit forcibly makes the current command zero, and by the current control circuit,
25 the voltage command by which the current detection value is made zero, is calculated, and when its voltage level is lower than the set voltage level, after the set level DC current

command is applied for a set time period from zero, the current command is forcibly made zero again, and by the current control circuit, even when the voltage command by which the current detection value is made zero, is calculated, when that

5 voltage level is lower than the set voltage level, the speed estimation circuit estimates that the AC motor is stopped.

(7) A control method of an AC motor according to any one of (1) to (6), wherein the start control circuit forcibly makes the current command zero, and by the current control circuit,
10 the voltage command so that the current detection value is made zero, is calculated, and by the time change of the voltage command, the speed estimation circuit starts the AC motor when the estimated AC motor speed and the amplitude and the phase of the voltage command are made the initial value.

15 (8) A control method of an AC motor according to any one of (1) to (7), wherein the start control circuit forcibly makes the current command zero, and by the current control circuit, the voltage command so that the current detection value is made zero, is calculated, and by the time change of the voltage
20 command, when the speed estimation circuit starts the AC motor when the estimated AC motor speed and the amplitude and the phase of the voltage command are made the initial value, until the amplitude of the voltage command outputted from the electric power converter is brought into the voltage level
25 corresponding to the normal induced voltage to the speed of the AC motor, the voltage command is gradually increased.

(9) A control apparatus of an AC motor which is characterized

in that: in the control apparatus of the AC motor which has the electric power converter to output an arbitrary electric power to the AC motor; the current detection circuit by which the current supplied to the motor is detected; the current
5 control circuit to control so that the given current command and the current detection value detected by the current detection circuit coincide with each other; and by which the switching of the electric power converter is determined from the voltage command outputted from the current control circuit,
10 the apparatus has the start control circuit, and the speed estimation circuit by which the speed of the AC motor in the free run condition is estimated.

(10) A control apparatus of an AC motor according to (9), wherein the start control circuit forcibly makes the current
15 command zero, and by the current control circuit, the voltage command so that the current detection value is made zero is calculated, and by the time change of the voltage command, the speed estimation circuit estimates the speed of the AC motor.

(11) A control apparatus of an AC motor according to either
20 one of (9) or (10), wherein the start control circuit forcibly makes the current command zero, and by the current control circuit, the voltage command so that the current detection value is made zero is calculated, and when its voltage level is lower than the set voltage level, after the set level DC
25 current command is applied for a set time period from zero, the current command is forcibly made zero again, and by the current control circuit, the voltage command so that the

current detection value is made zero, is calculated, and the speed estimation circuit estimates the speed of the AC motor.

(12) A control apparatus of an AC motor according to any one of (9) to (11), wherein the start control circuit forcibly makes
5 the current command zero, and by the current control circuit, the voltage command so that the current detection value is made zero is calculated, and when its voltage level is lower than the set voltage level, after the set level DC current command is applied for a set time period from zero, the current command
10 is forcibly made zero again, and by the current control circuit, even when the voltage command so that the current detection value is made zero, is calculated, when its voltage level is lower than the set voltage level, the speed estimation circuit estimates that the AC motor is stopped.

15 (13) A control apparatus of an AC motor according to any one of (9) to (12), wherein the start control circuit forcibly makes the current command zero, and by the current control circuit, the voltage command by which the current detection value is made zero, is calculated, and by the time change of the voltage
20 command, the speed estimation circuit makes the estimated speed of the AC motor and the amplitude and phase of the voltage command the initial value, and starts the AC motor.

(14) A control apparatus of an AC motor according to any one of (9) to (13), wherein the start control circuit forcibly makes
25 the current command zero, and by the current control circuit, the voltage command by which the current detection value is made zero, is calculated, and by the time change of the voltage

command, when the speed estimation circuit makes the estimated speed of the AC motor and the amplitude and phase of the voltage command the initial value, and starts the AC motor, the amplitude of the voltage command outputted from the electric power converter is gradually increased up to the voltage level corresponding to the normal induced voltage to the speed of the AC motor.

(15) A control method of an AC motor according to (3), wherein the start control circuit forcibly makes the current command zero, and by the current control circuit, the voltage command by which the current detection value is made zero, is calculated, and when the voltage command is larger than the set voltage level, by the time change of the phase of the voltage command, the speed estimation circuit estimates the speed of the AC motor, and as the initial value when the electric power converter is started, the amplitude and phase of the voltage command and the frequency corresponding to the speed estimation value of the AC motor are set, and the electric power converter is started.

(16) A control method of an AC motor which is characterized in that: the apparatus has an electric power converter to output the electric power to the AC motor; the current control section to control the output current of the electric power converter based on the difference signal of the current command signal and the output current detection signal of the electric power converter; and when the AC motor is in the free run condition, the arbitrary DC current is supplied to the AC motor for a set

time period, and the frequency component appeared in the output current detection signal of the electric power converter is detected, and from the frequency component, the speed of the AC motor is estimated.

5 (17) A control method of an AC motor according to (3), wherein the start control circuit forcibly makes the current command zero, and by the current control circuit, the voltage command by which the current detection value is made zero, is calculated, and when its voltage level is lower than the set voltage level,
10 the set level DC current command or the set level DC voltage command is applied for a set time period from zero, and the speed estimation circuit detects the frequency component appeared in the current detection value, and this frequency component is estimated as the speed of the AC motor, and as
15 the initial value when the electric power converter is started, the frequency corresponding to the speed estimation value of the AC motor is set, and the electric power converter is started.

20 (18) A control method of an AC motor according to (3), wherein the start control circuit forcibly makes the current command zero, and by the current control circuit, the voltage command by which the current detection value is made zero, is calculated, and when the voltage command is lower than the set voltage level, the current command value is changed from zero to the set level
25 DC current command value, and this is applied for a set time period, and after that, the sign and amplitude of the current command are changed, and it is applied for a set time period.

A control method of an AC motor is characterized in that, at this time, the speed estimation circuit detects the frequency component appeared in the current detection value, and it estimates the frequency component as the speed of the AC motor, and as the initial value when the electric power converter is started, the frequency corresponding to the speed estimation value of the AC motor is set, and the electric power converter is started.

(19) A control method of an AC motor according to (3), wherein the start control circuit forcibly makes the current command zero, and by the current control circuit, the voltage command by which the current detection value is made zero, is calculated, and when the voltage command is lower than the set voltage level, the current control is stopped, and the DC voltage command is applied in the arbitrary direction for a set time period, and after that, the arbitrary amplitude current command is given in the direction in which the phase is changed by 180° from the command direction of the DC voltage, and the current control is conducted again for a set time period. A control method of an AC motor characterized in that, at this time, the speed estimation circuit detects the frequency component appeared in the current detection value, and estimates the frequency component as the speed of the AC motor, and as the initial value when the electric power converter is started, the frequency corresponding to the speed estimation value of the AC motor is set, and the electric power converter is started.

(20) A control apparatus of an AC motor according to (9),

wherein the start control circuit forcibly makes the current command zero, and by the current control circuit, the voltage command by which the current detection value is made zero, is calculated, and when the voltage command is larger than the set voltage level, by the time change of the phase of the voltage command, the speed estimation circuit estimates the speed of the AC motor, and as the initial value when the electric power converter is started, the amplitude and phase of the voltage command and the frequency corresponding to the speed estimation value of the AC motor are set, and the electric power converter is started.

(21) A control apparatus of an AC motor according to (9), wherein the start control circuit forcibly makes the current command zero, and by the current control circuit, the voltage command by which the current detection value is made zero, is calculated, and when the voltage command is lower than the set voltage level, the set level DC current command, or the set level DC voltage command is applied for a set time period from zero, and the speed estimation circuit detects the frequency component appeared in the current detection value, and estimates the frequency component as the speed of the AC motor, and as the initial value when the electric power converter is started, the frequency corresponding to the speed estimation value of the AC motor is set, and the electric power converter is started.

(22) A control apparatus of an AC motor according to (9), wherein the start control circuit forcibly makes the current

command zero, and by the current control circuit, the voltage
command by which the current detection value is made zero, is
calculated, and when the voltage command is lower than the set
voltage level, the current command value is changed from
5 the zero to the set level DC current command value, and it is
applied for a set time period, and after that, the sign and
the amplitude of the current command are changed, and applied
for a set time period. The control apparatus of the AC motor
is characterized in that, at this time, the speed estimation
10 circuit detects the frequency component appeared in the current
detection value, and estimates the frequency component as the
speed of the AC motor, and as the initial value when the electric
power converter is started, the frequency corresponding to the
speed estimation value of the AC motor is set, and the electric
15 power converter is started.

(23) A control apparatus of an AC motor according to (3),
wherein the start control circuit forcibly makes the current
command zero, and by the current control circuit, the voltage
command by which the current detection value is made zero, is
20 calculated, and when the voltage command is lower than the set
voltage level, the current control is stopped, and the DC
voltage command is applied in the arbitrary direction for a
set time period, and after that, the arbitrary amplitude
current command is given in the direction in which the phase
25 is changed by 180° from the command direction of the DC voltage,
and the current control is conducted again for a set time period.
The control apparatus of the AC motor characterized in that,

at this time, the speed estimation circuit detects the frequency component appeared in the current detection value, and estimates the frequency component as the speed of the AC motor, and as the initial value when the electric power
5 converter is started, the frequency corresponding to the speed estimation value of the AC motor is set, and the electric power converter is started.

Brief Description of the Drawings

10 Fig. 1 is a block diagram of a variable speed control apparatus of an AC motor according to the first embodiment of the present invention.

Fig. 2 is a block diagram showing the structure of a 2 phase/3 phase converter shown in Fig. 1.

15 Fig. 3 is a view showing the operation wave form at the time of free run condition of the AC motor shown in Fig. 1.

Fig. 4 is a block diagram of the variable speed control apparatus of the AC motor according to the second embodiment of the present invention.

20 Fig. 5 is a block diagram of the control apparatus of the AC motor according to the third embodiment of the present invention.

Fig. 6 is a diagram showing the relationship between the locus of the residual voltage of the AC motor and the output
25 voltage command and phase (at the time of normal rotation) of a current controller.

Fig. 7 is a diagram showing the relationship between the

locus of the residual voltage of the AC motor and the output voltage command and phase (at the time of reverse rotation) of the current controller.

Fig. 8 is a block diagram of the control apparatus of the AC motor according to the fourth embodiment of the present invention.

Figs. 9(a) to 9(c) show the diagrams showing a variation (normal rotation) of the current detection value when a d-axis voltage is given to the AC motor.

Figs. 10(a) to 10(c) show the diagrams showing a variation (reverse rotation) of the current detection value when the d-axis voltage is given to the AC motor.

Fig. 11 is a block diagram of the control apparatus of the AC motor according to the fifth embodiment of the present invention.

Fig. 12 is a diagram showing a variation (normal rotation) of a torque current detection value when an exciting current command is given to the AC motor.

Fig. 13 is a diagram showing a variation (reverse rotation) of the torque current detection value when the exciting current command is given to the AC motor.

In this connection, as a reference numeral in the drawings, numeral 1 is an electric power converter, numeral 2 is a current vector control circuit, numeral 3 is a 3 phase/2 phase converter, numeral 4 is a primary angular frequency calculation circuit, numeral 5 is an exciting current control circuit, numeral 6 is a torque current control circuit, numeral

7 is a 2 phase/3 phase converter, numeral 8 is a voltage pattern producer, numeral 9 is an AC motor, numeral 10 is an integrator, numeral 11 is an instantaneous power failure re-start control circuit, numeral 12 is a magnetizing current command switching unit, numeral 13 is a torque current switching unit, numeral 14 is a phase command switching unit, numeral 15 is a signal holding circuit, numeral 70 is a voltage command amplitude calculator, numeral 71 is a voltage command phase calculator, numeral 72 is a voltage command converter, numeral 201 is an electric power converter, numeral 202 is an AC motor, numeral 203 is a current detector, numeral 204 is a current coordinate converter circuit, numeral 205 is a torque current control circuit, numeral 206 is an exciting current control circuit, numeral 207 is a phase calculation circuit, numeral 208 is a V/f converter circuit, numeral 209 is an output voltage calculation circuit, numeral 210 is a switching pattern generation circuit, numeral 211 is an instantaneous power failure re-start control circuit, numeral 212 is a speed estimation circuit, numeral 212A is a speed estimation circuit(when the residual voltage exists), and numeral 212B is a speed estimation circuit (when no residual voltage exists).

Best Mode for Carrying Out the Invention

Referring to the drawings, the present invention will be described below. Initially, referring to Fig. 1 to Fig. 3, the first embodiment of the present invention will be

described. Fig. 1 is a block diagram of the variable speed control apparatus of an AC motor according to the first embodiment of the present invention, and Fig. 2 is a block diagram showing a structure of a 2 phase/3 phase converter shown in Fig. 1. Further, Fig. 3 is a view showing an operation waveform in the free run condition of the AC motor shown in Fig. 1.

In Fig. 1, in the variable speed control apparatus, an electric power converter 1 by which, after an AC power source from the 3 phase AC power source is converted into a DC power, it is converted again into the AC power of an arbitrary frequency and voltage by an inverter by the PWM control system, and this primary frequency and the primary voltage are supplied to an AC motor 9; a current vector control circuit 2 by which, a speed command signal ω_r ref inputted from the outside is inputted, and from an exciting current detection value i_{dfb} outputted from a 3 phase/2 phase converter 3 and a torque current detection value i_{qfb} , a speed estimation signal ω_r is obtained; the 3 phase/2 phase converter 3 by which the primary current (U phase current i_u , W phase current i_w) to the AC motor 9 is detected, and the exciting current detection value i_{dfb} which is coordinate-transformed, and the torque current detection value i_{qfb} are sent out; a primary angular frequency calculation circuit 4 by which, from the speed estimation signal ω_r from the current vector control circuit 2, it is calculated into the primary angular frequency signal ω_1 and outputted; an exciting current control circuit (ACR d) 5 by

which the exciting current directional voltage provided so that the exciting current command value $i_d \text{ ref}$ and the exciting current detection value i_{dfb} from the 3 phase/2 phase converter 3 coincide with each other, is controlled; a torque current control circuit (ADR q) 6 by which the torque current directional voltage provided so that the torque current command value $i_q \text{ ref}$ outputted from the current vector control circuit 2 and the torque current detection value i_{qfb} outputted from the 3 phase/2 phase converter 3 coincide with each other, is controlled; a 2 phase/3 phase converter 7 by which the PWM signal of the voltage command signal (V_{uref} , V_{vref} , V_{wref}) of each phase of U, V, W is generated and outputted; a V/f converter circuit 208 by which the induced voltage command signal E_{ref} is made so that the induced voltage of the AC motor is compensated based on the primary angular frequency signal ω_1 from a primary angular frequency calculation circuit 4; an integrator 10 by which the primary angular frequency signal ω_1 from the primary angular frequency calculation circuit 4 is integrated in the same manner; an instantaneous power failure detection re-start control circuit 11 by which, after the instantaneous power failure is detected, the procedure up to the re-running is controlled; a magnetizing current command switching unit 12 by which, by the instantaneous power failure signal from the instantaneous power failure detection re-start control circuit 11, the exciting current command value is switched; a torque current command switching unit 13 by which, in the same manner, by the instantaneous power failure signal,

the torque current command value is switched; and a phase command switching unit 14 by which, in the same manner, by the instantaneous power failure signal, the phase command signal is switched, are provided.

5 In this connection, the output signal of the exciting current control circuit (ACR d) 5 becomes the d-axis voltage command value V_{dref} , and the additional value of the output signal of the torque current control circuit (ACR q) 6 and the output signal E_{ref} of the V/f converter circuit 208 becomes
10 the q-axis voltage command value V_{qref} . Further, the output signal of the integrator 10 is inputted into the 3 phase/2 phase converter 3 and the 2 phase/3 phase converter 7 as the phase command signal θ . In Fig. 2, a voltage command amplitude calculator 70 which calculates the amplitude $|V_1|$ of the output
15 voltage command signal V_1 , as $|V_1| = (V_{dref}^2 + V_{qref}^2)^{1/2}$, from the d-axis voltage command value V_{dref} and the q-axis voltage command value V_{qref} , a voltage command phase calculator 71 which calculates the phase signal γ of the output voltage command signal V_1 , as $\gamma = \tan^{-1} (V_{qref}/V_{dref})$, and a voltage
20 command converter 72 which converts them into the voltage command signals V_{uref} , V_{vref} , V_{wref} of each phase of the U, V, W, from the amplitude $|V_1|$ of the output voltage command signal V_1 and phase γ and inputted phase command signal θ , as $V_{uref} = |V_1| \times \cos (\theta + \gamma)$, $V_{vref} = |V_1| \times \cos (\theta + \gamma + 120^\circ)$, and V_{wref}
25 $= |V_1| \times \cos (\theta + \gamma + 240^\circ)$, are provided.

Next, the operation will be described as follows.

The voltage command signal when the current of the AC

motor 9 is zero coincides with the residual voltage of the AC motor. Because, the current flows between 2 points between which the potential difference exists. Accordingly, the status in which the current between the electric power

5 converter 1 and the AC motor 9 is zero, shows that, between the output voltage of the electric power converter 1 and the voltage of the AC motor 9, the potential difference does not exist, that is, they are at the same voltage value. In this case, the 2 axes perpendicular to each other, that is, because
10 the current control is individually conducted by separating them into the exciting current and torque current directions, in each component voltage of the 2 axes perpendicular to each other, the output of the electric power converter 1 and the voltage of the AC motor 9 are also coincide with each other.

15 As the result, in the residual voltage of the AC motor 9, aiming that the respective component voltage of the 2 axes perpendicular to each other appears as the d-axis voltage command value V_{dref} and q-axis voltage command value V_{qref} , in the present embodiment, the phase and angular velocity of

20 the residual voltage of the AC motor are detected, and the re-start operation at the time of the instantaneous power failure is conducted. In the specific operation when the re-start is conducted at the time of recovery of power after the instantaneous power failure is generated, when the

25 instantaneous power failure re-start control circuit 11 detects the instantaneous power failure, the instantaneous power failure signal is inputted into the magnetizing current

command switching unit 12, torque current switching unit 13,
and phase command switching unit 14. When the instantaneous
power failure signal is inputted, the magnetizing current
command switching unit 12 switches the exciting current command
5 value i_{dref} into zero, and in the same manner, torque current
switching unit 13 switches the torque current command value
 i_{qref} into zero, and phase command switching unit 14 switches
the phase command signal θ into zero. Accordingly, the output
as the following expressions is conducted.

10 $i_{dref} = 0$
 $i_{qref} = 0$
 $\theta = 0$

After the above operation, when the current control is
conducted by the exciting current control circuit 5 and the
15 torque current control circuit 6, the current control is
conducted so that the current of the AC motor 9 becomes zero.
When the current of the AC motor 9 becomes zero by the current
control, the voltage is balanced, and the component voltage
of 2 perpendicular axes of the residual voltage of the AC motor
20 9 appear as the d-axis voltage command value V_{dref} and the
q-axis voltage command value V_{qref} .

Because the output γ of the voltage command phase
calculator 71 shown in the drawing, into which this d-axis
voltage command value V_{dref} and the q-axis voltage command
25 value V_{qref} are inputted, coincides with the phase of the
residual voltage of the AC motor 9, the phase of the residual
voltage of the AC motor 9 can be easily obtained by the output

γ of the voltage command phase calculator 71, and the angular velocity of the residual voltage can be easily obtained by the changing amount per unit time of the output γ of the voltage command phase calculator 71. In the same manner, this d-axis voltage command value V_{dref} and the q-axis voltage command value V_{qref} are the input. The output $|V_1|$ of the voltage command amplitude calculator 70 shown in Fig. 2 coincides with the amplitude of the residual voltage. When the above operations are completed, the instantaneous power failure re-start control circuit 11 sets the output γ of the voltage command phase calculator 71 as the initial value to the integrator 10, and sets the changing amount per unit time of the output γ of the voltage command phase calculator 71 to the speed estimation signal ω_r in the current vector control circuit 2, and sets the output $|V_1|$ of the voltage command amplitude calculator 70 to the E_{ref} of the output of the V/f converter circuit 208, and the relief signal of the instantaneous power failure signal is respectively inputted into the magnetizing current command switching unit 12, torque current switching unit 13, and phase command switching unit 14. After the magnetizing current command switching unit 12 and torque current switching unit 13 respectively switch the exciting current command value i_{dref} and torque current command value i_{qref} to each current command signal which is the output signal of the current vector control circuit 2, and the phase command switching unit 14 switches the phase command signal θ to the output signal of the integrator 10, they are operated

again, and continuously drive the AC motor 9.

Fig. 3 is an example of the operation waveform when the operation principle as described above is applied to the AC motor 9 which is free-run in the normal rotation direction, and Fig. 3(a) is a voltage command signal waveform, and Fig. 3(b) is a view showing the phase γ . As shown in Fig. 3(a), when the AC motor 9 is in the normal rotation, the d-axis voltage command value V_{dref} advances by the phase 90° to the q-axis voltage command value V_{qref} , and the amplitudes of respective voltage signals attenuate as the passage of time. Further, in the case of Fig. 3(b), it is the case where the output γ of the voltage command phase calculator 71 is rotated in the positive side. Further, although not shown, when the AC motor 9 is in the reverse rotation, the d-axis voltage command value V_{dref} is delayed by the phase 90° to the q-axis voltage command value V_{qref} , and the amplitude of respective voltage signals attenuates as the passage of time in the same manner, and the output γ of the voltage command phase calculator 71 is rotated in the reverse side. In this connection, up to this case, it is described that, when the current of the AC motor 9 becomes zero, the residual voltage of the AC motor 9 appears as the d-axis voltage command value V_{dref} and the q-axis voltage command value V_{qref} , however, even when the current of the AC motor 9 does not perfectly become zero, the detection of the phase and angular velocity can be conducted.

Next, referring to Fig. 4, the second embodiment of the present invention will be described. Fig. 4 is a block diagram

of the variable speed control apparatus of the AC motor according to the second embodiment of the present invention. The second embodiment shown in Fig. 4 is an improved example to avoid the disadvantages because the disadvantages are
5 generated sometimes, in which, in the operation of previous embodiment shown in Fig. 1, in order to switch the phase command switching unit 14 to zero at the time of generation of the instantaneous power failure, the phase command signal θ becomes discontinuous, thereby, the mechanical shock is generated, or
10 the DC voltage of the electric power converter 1 becomes the over voltage, thereby, the variable speed control apparatus trips. In the second example in Fig. 4, the different structure from Fig. 1 is as follows: by the instantaneous power failure signal outputted from the instantaneous power failure re-start
15 control circuit 11, in place of making the phase command signal θ zero, a new signal holding circuit 15 is provided, and in the signal holding circuit 15, the primary angular frequency signal ω_1 is held, and the held value is inputted into the V/f converter circuit 208, and the integrator 10, and when re-
20 started by the recovery of power failure, in place of the case in which the phase of the AC motor 9 is obtained by the output γ of the voltage command calculator 71, and the angular velocity of the residual voltage is obtained by the changing amount per unit time of the output γ , the phase of the residual voltage
25 of the AC motor 9 is obtained by the addition value of the output γ of the voltage command calculator 71 and the phase command signal θ , and the angular velocity of the residual voltage is

obtained by the changing amount per unit time of the addition value of the output γ and the phase command signal θ . In this connection, other same structures as in Fig. 1 are denoted by the same reference numbers, and double explanations will be neglected.

Next, the operation will be described.

In also the structure in Fig. 4, in the same manner as in Fig. 1, at the time of the instantaneous power failure, the current of the magnetizing current command switching unit 12 and the torque current switching unit 13 is switched into zero by the instantaneous power failure signal, and by the exciting current control circuit 206 and the torque current control circuit 6, the current control is conducted so that the current of the AC motor 9 becomes zero, and because the voltage component of 2 perpendicular axes of the residual voltage appears as the d-axis voltage command value V_{dref} and the q-axis voltage command value V_{qref} , and as shown in Fig. 2, the phase of the residual voltage of the AC motor is obtained by the addition value $(\theta + \gamma)$ of the output γ of the voltage command phase calculator 71 and the phase command signal θ , and the angular velocity is obtained by the changing amount per unit time of the addition value $(\theta + \gamma)$. In this case, because the primary angular frequency ω_1 is switched to the held side by the signal holding circuit 15 at the time of instantaneous power failure, the primary angular frequency ω_1 from the signal holding circuit 15 is added to the integrator 10, and the phase command signal θ is continuously outputted from the integrator

10, and the addition value $(\theta + \gamma)$ is obtained. By this operation, because the discontinuous operation of the phase command signal θ at the time of instantaneous power failure occurrence does not exist, the occurrence of the mechanical shock or the trip
5 of the variable speed control apparatus can be avoided.

Further, in the re-start after the power recovery, by conducting the same recovery procedure as in Fig. 1, when the re-start is conducted and the AC motor 9 is driven, the quick and smooth re-start becomes possible, and the situation in
10 which the inverter stop by the instantaneous power failure results in the stop of the whole equipments of the production line, and the damage is expanded, can be avoided.

In this connection, in the present invention, in order to remove the discontinuity of the phase command signal θ at
15 the generation time of the instantaneous power failure, the holding circuit 15 is provided, thereby, the primary angular frequency is held, however, in place of the holding circuit 15, a command switching unit is provided, and at the generation time of the instantaneous power failure, even when the primary
20 angular frequency is also switched to zero, because the discontinuity of the phase command signal θ can be removed, the same effect as in the present invention can be obtained.

Further, in the present invention, hitherto, the variable speed control apparatus to conduct the vector control
25 in which the exciting current of the AC motor 9, and the torque current are respectively independently controlled, is described, however, in also the variable speed control

apparatus to conduct the V/f constant control, at the time of re-start after the instantaneous power failure, in the case where the current control section by which the exciting current of the AC motor and the torque current are respectively

5 independently controlled, is added, when the primary current is circulated and the magnetic flux of the AC motor is built up, the present invention can be conducted in the same manner.

Next, the third embodiment of the present invention will be described. Fig. 5 is a block diagram showing the structure
10 of the third embodiment of the control apparatus of the AC motor in the present invention. The control apparatus of the motor in the present embodiment is provided with: the electric power converter 201; AC motor 202; current detector 203; current coordinate conversion circuit 204; torque current control
15 circuit 205; exciting current control circuit 206; phase calculation circuit 207; V/f converter circuit 208; output voltage calculation circuit 209; switching pattern generation circuit 210; instantaneous power failure re-start control circuit 211; and speed estimation circuit 212. The electric
20 power converter 201 converts the DC voltage into which the 3 phase AC is converted by the power element, into the AC of the arbitrary frequency f_1 and voltage by the PWM control system, and supplies it to the AC motor 202. The current detector 203 detects the current supplied to the AC motor 202.

25 The current coordinate conversion circuit 204 separates the current detected by the current detector 203 into the torque current detection value i_{qfb} and the exciting current detection

The torque current control circuit 205 calculates the first q-axis voltage command value V'_{qref} so that the given torque current command value i_{qref} and the torque current detection value i_{dfb} coincide with each other.

10 The phase calculation circuit 207 calculates the phase
 θ by integrating the given frequency f_1 .

15 The output voltage calculation circuit 209 adds the first
q-axis voltage command value V'_{qref} which is the output of the
torque current control circuit 205 and the voltage e which is
the output of the V/f converter circuit 208, and calculates
the second q-axis voltage command value V_{qref} , and from the
20 second q-axis voltage command value V_{qref} and the d-axis
voltage command value V_{dref} , the output voltage command value
 V_{lref} and its voltage phase θ_v are outputted.

The switching pattern generation circuit 210 determines the switching pattern of the electric power converter 1 from the electric power converter output phase θ_{deg} in which the output voltage command value V_{lref} and the voltage phase θ_v and the phase θ are added..

The instantaneous power failure control circuit 211 controls the electric power converter 201 so that it is normally operated, when the power source recovers and re-starts, or the operation command is inputted and started, after the detection
5 of the instantaneous power failure.

The speed estimation circuit 212 is a circuit to estimate the speed fr of the AC motor 2 in the free run condition.

Next, before explaining the operation principle of the
10 re-start method at time of instantaneous power failure occurrence, by using the relationship of the locus of the residual voltage in Fig. 6, and the voltage command and phase, the method to estimate the speed of the AC motor 202 in the free run condition will be described. The AC motor 202 in the
15 free run condition at the time of the instantaneous power failure during the normal operation generates the residual voltage, and the locus of the voltage is rotated as the left view at the rotation speed of the AC motor 202. Therefore, when the electric power converter 201 is started to be operated
20 irrespective of the condition of the AC motor 202, the current circulates between the AC motor 202 and the electric power converter 201. However, when the residual voltage of the AC motor 202 and the amplitude, phase and frequency of the output voltage of the electric power converter coincide with each
25 other, the current does not circulate. In order to make the current circulating between the electric power converter 201 and the AC motor 202 zero, the torque current command value

igref and the exciting current command value idref and frequency f1 are set to zero, and in the torque current control circuit 205, and exciting current control circuit 206, it may be controlled so that the torque current detection value iqfb and exciting current detection value idfb flowing to the AC motor 202 respectively coincide with the command values. This is called the zero current control. The first q-axis voltage command value V'_{qref} and d-axis voltage command value v_{dref} which are the output of the torque current control circuit 205, and the exciting current control circuit 206 at the time of the zero current control, become the sinusoidal voltage command values of the frequency f1 which coincides with the rotation speed of the AC motor 202 as shown in Fig. 6(b) upper side view.

When the frequency f1 is set to zero, the phase θ outputted from the phase calculation circuit 207 is fixed, and the voltage E_{ref} outputted from the V/f converter circuit 208 becomes zero.

The output voltage calculation circuit 209 has the first q-axis voltage command value V'_{qref} and the d-axis voltage command value V_{dref} as the inputs, and outputs the output voltage command value V_{lref} and the voltage phase θ_v . The output voltage command value V_{lref} expresses the amplitude of the residual voltage, and the voltage phase θ_v expresses the phase of the residual voltage.

Therefore, as shown in Fig. 6(b) lower side view, when the time change of the phase of the residual voltage is measured at every time, the speed estimation circuit 212 measures the frequency of the residual voltage. Because the frequency of

the residual voltage coincides with the rotation speed of the AC motor 202, the rotation speed of the AC motor 202 in the free run condition can be estimated. Although Fig. 6 is considered about the case where the AC motor is normally rotated, 5 when the AC motor is reversely rotated, because only the rotation direction of the phase of the residual voltage is different, it can be considered in the same manner. This is shown in Fig. 7. In this manner, when the residual voltage is measured, including the rotation direction of the AC motor, 10 the rotation speed can be estimated.

Next, the operation when the re-start is conducted at the time of the power recovery after the instantaneous power failure, will be described. When the instantaneous power 15 failure occurs during the operation of the AC motor 202, the electric power converter 201 stops the operation, and the AC motor 202 is in the free run condition. When the power is recovered, and the electric power converter 201 is in the operable condition, the instantaneous power failure re-start 20 circuit 211 forcibly makes the torque current command value i_{qref} and the exciting current command value i_{dref} and the frequency zero. Then, the zero current control is conducted, and the output voltage command value V_{lref} and its voltage phase θ_v which are the amplitude and phase of the residual voltage 25 of the AC motor 202, are calculated from the output voltage calculation circuit 209.

The instantaneous power failure re-start control circuit

211, when the output voltage command value V_{lref} outputted from the output voltage calculation circuit 209 is larger than the arbitrary set voltage level, makes the voltage phase θ_v the input, and the speed estimation circuit 212 controls that the
5 estimation value fr of the rotation speed of the AC motor is outputted.

When the output voltage command value V_{lref} outputted from the output voltage calculation circuit 209 is smaller than the arbitrary set voltage level, because the AC motor 202 is
10 stopped or rotated at the low speed, it can not be judged whether the output voltage command value V_{lref} is small, or the AC motor is rotated at the high speed, but the residual voltage is reduced small, because the instantaneous power failure time is longer than the secondary constant of the AC motor.
15 Therefore, the instantaneous power failure re-start control circuit 211 flows the arbitrary level DC current for an arbitrary set time, and tries the excitation again, and the zero current control is conducted once more, and calculates the output voltage command value V_{lref} and its voltage phase
20 θ_v which are the amplitude and phase of the residual voltage of the AC motor 202, from the output voltage calculation circuit 209.

Then, when the output voltage command value V_{lref} outputted from the output voltage calculation circuit 209 is
25 larger than the arbitrarily set voltage level, the instantaneous power failure re-start control circuit 211 makes the voltage phase θ_v as the input, and the speed estimation

circuit 212 controls that the estimation value ω_r of the rotation speed of the AC motor is outputted.

After the re-exciting is conducted, when the output voltage command value V_{lref} outputted from the output voltage calculation circuit 209 is smaller than the arbitrarily set voltage level, the instantaneous power failure re-start control circuit 211 makes the voltage phase θ_v as the input, and the speed estimation circuit 212 controls that it is judged that the AC motor is stopped. As described above, the instantaneous power failure re-start control circuit 211 observes the output voltage command value V_{lref} outputted from the output voltage calculation circuit 209, and when the speed estimation circuit 212 makes the speed of the AC motor as the output value of the estimation value, the instantaneous power failure re-start control circuit 211 stops the zero current control, and enters in the normal operation condition. When the condition is shifted from the zero current control condition to the normal operation, even when only the frequency f_1 is made to coincide and the electric power converter 201 is started, the over current flows in the AC motor, thereby, there is a possibility that the smooth start can not be conducted. In order to prevent this, the amplitude and phase of the residual voltage in the zero current control may be continued even at an instance when the zero current control is shifted to the normal operation. The instantaneous power failure re-start control circuit 211 controls that the initial value is set to the output voltage command value V_{lref} of the

electric power converter and the electric power converter
output phase θ deg and output frequency f_1 . The output voltage
command value V_{lref} of the electric power converter sets the
output voltage command value V_{lref} calculated by the output
5 voltage calculation circuit 209 in the zero current control.
Herein, because the residual voltage measured by the zero
current control is the induced voltage e of the AC motor 202,
as the initial value of the output voltage E_{ref} of the V/f
converter 208, the output voltage command value V_{lref}
10 calculated by the output voltage calculation circuit 209 is
set in the zero current control. The initial value of the
output frequency f_1 sets the estimation value f_r of the rotation
speed of the AC motor 202 outputted by the speed estimation
circuit 212.

15 In the normal operation condition, although the electric
power converter output phase θ deg is controlled on the basis
of the phase of the magnetic flux of the AC motor 202, during
the zero current control, because the phase of the induced
voltage e of the AC motor 202 is outputted, the phase advances
20 by 90° at the time of normal rotation, and the phase is delayed
by 90° at the time of reverse rotation. Accordingly, the
initial value of the electric power converter output phase θ
deg, after the phase is corrected by 90° corresponding to the
rotation direction from the last phase of the zero current
25 control, the value in which the advanced amount of the phase
is corrected, by the estimation value f_r of the rotation speed
of the AC motor 202 outputted by the speed estimation circuit

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Next, by using the change of the current detection value when the d-axis voltage is given to the AC motor in Fig. 9, a method by which the speed of the AC motor 202 in the free run condition when no residual voltage exists, is estimated, will be described. The AC motor 202 in the free run condition at the time of the instantaneous power failure generates the residual voltage, however, when the instantaneous power failure time is longer than the secondary circuit time constant of the AC motor, the residual voltage disappears. In this case, in the third embodiment, the speed of the AC motor can not be estimated. Therefore, in the fourth embodiment, the exciting current is circulated in to the AC motor in the free run, and the frequency f_1 of the secondary current transiently circulating in the rotor when the magnetic flux is built up is detected, and the speed of the AC motor is estimated.

Initially, in order to excite the AC motor, a set value is given to the exciting current command id_{ref} , and zero is respectively given to the torque current command, and the exciting current control circuit 206 controls so that the exciting current detection value id_{fb} coincides with the exciting current command id_{ref} . In order to obtain the motor speed information, the torque current control circuit 205 does not control. When if the motor is in the stopped condition, because the voltage necessary for the d-axis is only the primary resistance drop voltage, the primary resistance drop voltage is given to the d-axis voltage command V_d^* as the initial value,

and the q-axis voltage command V_q^* is made zero. Because the speed of the AC motor is unknown, the frequency is also made zero. This is equivalent to a case where the DC voltage command V_{dref} is given to an arbitrary phase. In this case, when the AC motor 2 is rotated, the torque current detection value i_{qfb} changes as in Fig. 9. The frequency of the torque current detection value i_{qfb} coincides with the speed of the AC motor 202 in the free run condition. When the frequency of this torque current detection value i_{qfb} is measured, the speed of the AC motor 202 can be detected.

In Fig. 9, although a case where the AC motor is normally rotated, is considered, but in a case where the AC motor is reversely rotated, the relationship between the phases of the exciting current detection value i_{dfb} and the torque current value i_{qfb} is different. This is shown in Fig. 10.

In this manner, in the case of normal rotation, the exciting current detection value i_{dfb} is more advanced than the torque current detection value i_{qfb} , and in the case of reverse rotation, the exciting current detection value i_{dfb} is more delayed than the torque current detection value i_{qfb} . In this manner, when the DC voltage is applied, the rotation speed can be estimated including the rotation direction of the AC motor.

When the free run speed of the motor is low, because the amplitude is hardly generated in the exciting current detection value i_{dfb} , the rotation direction can not be detected only by this method. However, when the motor is rotated, the

sinusoidal signal appears in the torque current detection value i_{qfb} . In the case of the normal rotation, the sinusoidal signal begins from the phase 180° , and in the case of reverse rotation, it begins from the phase 0° . In this manner, the rotation
5 direction can be detected depending on from which phase it begins.

The operation in the case where the electric power is recovered after the instantaneous power failure occurs, will
10 be described. When the instantaneous power failure occurs while the AC motor 202 is operated, the electric power converter 201 stops the operation, and the AC motor 202 becomes the free run condition. When the power source recovers and the electric power converter 201 becomes the operable condition, the
15 instantaneous power failure re-start circuit 211 makes the torque current command value i_{qref} and the exciting current command value i_{dref} and the frequency f_1 forcibly zero. Then, the zero current control is conducted, and from the output voltage calculation circuit 209, the output voltage command
20 value V_{lref} and its voltage phase θ_v which are the amplitude and the phase of the residual voltage of the AC motor 2, are calculated.

When the output voltage command value V_{lref} outputted from the output voltage calculation circuit 209 is smaller than
25 the arbitrarily set voltage level, the instantaneous power failure re-start control circuit 211 can not judge that, because the AC motor 202 stops or is rotated at low speed,

whether the output voltage command value V_{lref} is small, or although the AC motor is rotated at high speed, because the instantaneous power failure time is longer than the secondary time constant of the AC motor, whether the residual voltage is decreased. Therefore, when the instantaneous power failure re-start control circuit 211 impresses the DC voltage of the arbitrary level for an arbitrarily set time period, the DC current flows, and the exciting current detection value i_{dfb} and the torque current detection value i_{qfb} are inputted into the speed estimation circuit 212B, and it is controlled that the estimation value of the rotation speed of the AC motor is outputted by the above described method. When the speed estimation circuit 212B outputs the speed estimation value of the AC motor, the instantaneous power failure re-start control circuit 211 stops the impression of the DC voltage, and enters into the normal operation. When the condition is shifted from the DC voltage impression condition to the normal operation, the frequency f_1 corresponding to the speed estimation value outputted from the speed estimation circuit 212B may be set to the electric power converter 201, however, when the AC motor is started by giving the voltage command which is the induced voltage corresponding to the rotation speed of the AC motor, the over current flows in the AC motor, and there is a possibility that the smooth start can not be conducted. In order to prevent this, the instantaneous power failure re-start control circuit 211 controls that the output voltage of the V/f converter 8 is gradually increased until it corresponds

to the normal induced voltage of the AC motor 202.

In the above described embodiments, it is considered that only the exciting current control circuit 206 is operated, however, only the torque current control circuit 205 may be operated, or neither current control circuits may also be
5 operated. Further, the DC voltage command may also be given to the q-axis direction.

Next, referring to the drawings, the fifth embodiment
10 of the present invention will be described. Fig. 11 is a block diagram showing the structure of the fifth embodiment of the control apparatus of the AC motor in the present invention. The control apparatus of the motor in the present embodiment is provided with: the electric power converter 201; AC motor
15 202; current detector 203; current coordinate conversion circuit 204; torque current control circuit 205; exciting current control circuit 206; phase calculation circuit 207; V/f converter circuit 208; output voltage calculation circuit 209; switching pattern generation circuit 210; instantaneous
20 power failure re-start control circuit 211, and speed estimation circuit 212.

The electric power converter 201 converts the DC voltage into which the 3 phase AC is converted by the power element, into the AC having an arbitrary frequency and voltage by the
25 PWM control system, and supplies it to the AC motor 202.

The current detector 203 detects the current supplied to the AC motor 202. The current coordinate conversion circuit

204 separates the current detected by the current detector 203 into the torque current detection value i_{qfb} and the exciting current detection value i_{dfb} . The torque current control circuit 205 calculates the first q-axis voltage command value V_{qref} so that the given torque current command value i_{qref} and the torque current detection value i_{qfb} coincide with each other.

The exciting current control circuit 206 calculates the d-axis voltage command value V_{dref} so that the given exciting current command value i_{dref} and the exciting current detection value i_{dfb} coincide with each other.

The phase calculation circuit 207 calculates the phase by integrating the given frequency f_1 .

The V/f conversion circuit 208 calculates the voltage E_{ref} corresponding to the induced voltage of the AC motor from the given frequency f_1 .

The output voltage calculation circuit 209 adds the first q-axis voltage command value V_{qref} which is the output of the torque current control circuit 5 to the voltage E_{ref} which is the output of the V/f converter circuit 208, and calculates the second q-axis voltage command value V_{qref} , and from the second q-axis voltage command value V_{qref} and the d-axis voltage command value V_{dref} , outputs the output voltage command value V_{lref} and its voltage phase θ_v .

The switching pattern generation circuit 210 determines the switching pattern of the electric converter 201 from the electric converter output phase θ_{deg} in which the output

voltage command value V_1 ref and the voltage phase θ_v and phase are added to each other.

The instantaneous power failure re-start control circuit 211 controls the electric converter 201 so that it is normally operated, after the instantaneous power failure is detected, when the re-start is conducted after the power source is recovered, or when the motor is started after the operation command is inputted.

The speed estimation circuit 212 is a circuit to estimate the speed ω_r of the AC motor in the free run condition.

Next, the method to estimate the speed of the AC motor 202 in the free run condition in the case of no residual voltage, will be described, by using the change of the current detection value when the d-axis voltage is given to the AC motor in Fig. 12. The AC motor 202 in the free run condition due to the instantaneous power failure generates the residual voltage, however, when the instantaneous power failure time is longer than the secondary circuit time constant of the AC motor, the residual voltage disappears. Therefore, in the second embodiment, the exciting current flows to the AC motor in the free run condition, and when the magnetic flux is built up, the frequency of the secondary current transiently flowing in the rotor is detected, thereby, the speed of the AC motor is estimated.

Initially, in order to excite the AC motor, a certain set value is given to the exciting current command i_d ref and the zero is respectively given to the torque current command

igref, and the exciting current control circuit 206 controls so that the exciting current detection value i_d coincides with the exciting current command i_{dref} for a set time period. After that, the sign and the amplitude of the exciting current command i_{dref} are changed, and the control is conducted for the set time period. In order to obtain the motor speed information, the torque current control circuit 205 is not controlled. The d-axis voltage command V_{dref} and the q-axis voltage command are made zero. Because the speed of the motor is unknown, the frequency is also made zero. In this case, when the AC motor 202 is rotated, the torque current detection value i_{qfb} changes as shown in Fig. 12. When the sign of the exciting current command is negative, the torque current detection value i_{qfb} is changed to the sinusoidal wave whose phase begins from 0° , and when the sign of the exciting current command is positive, the torque current detection value i_{qfb} is changed to the sinusoidal wave whose phase begins from 180° . The frequency of the sinusoidal wave of the torque current detection value i_{qfb} coincides with the speed of the AC motor 202 in the free run condition. By measuring the frequency of this torque current detection value i_{qfb} , the speed of the AC motor 202 can be detected.

Although, in Fig. 12, a case where the AC motor 202 is normally rotated, is considered, when the AC motor 202 is reversely rotated, the waveform as shown in Fig. 13 is obtained. As described above, when the sign of the exciting current command i_{dref} is positive, in the case of the normal rotation,

the phase of the torque current detection value i_{qfb} begins from 0° , and in the case of the reverse rotation, the phase begins from 180° . As described above, when the exciting current command i_{dref} is given and controlled, including the
5. rotation direction of the AC motor 202, the rotation speed can be estimated.

Next, the operation when the re-start is conducted due to the power recovery after the occurrence of the instantaneous power failure, will be described. When the instantaneous
10 power failure occurs during the operation of the AC motor, the electric power converter 201 stops the operation, and the AC motor 202 becomes the free run condition. When the power source is recovered, and the electric power converter 201 becomes the operable condition, the instantaneous power failure re-start
15 control circuit 211 forcibly makes the torque current command value i_{qref} and exciting current command value i_{dref} and frequency f_1 zero. Then, the zero current control is conducted, and from the output voltage calculation circuit 209, the output voltage command value V_{lref} and its voltage phase θ_v which are
20 the amplitude and phase of the residual voltage of the AC motor, are calculated. The instantaneous power failure re-start control circuit 211 can not judge, when the output voltage command value V_{lref} outputted from the output voltage
25 calculation circuit 209 is smaller than the arbitrarily set voltage level, because the AC motor 202 is stopped or rotated at the low speed, whether the output voltage command value V_{lref} is small, or whether, although the AC motor is rotated at high

speed, because the instantaneous power failure time is longer than the secondary time constant of the AC motor 202, the residual voltage becomes small. Therefore, after the instantaneous power failure re-start control circuit 211 gives
5 the DC current command to the exciting current command value i_{dref} for an arbitrarily set time period, the sign and amplitude of the DC current command are changed and the current control is conducted, and the torque current detection value i_q is inputted into the speed estimation circuit 212, and it is
10 controlled that, by the above described method, the estimation value of the rotation speed of the AC motor 202 is outputted.

The instantaneous power failure re-start control circuit 211 stops the current control when the arbitrarily set time is passed, and because the speed estimation circuit 212 outputs
15 the speed estimation value of the AC motor 202, it enters into the normal operation condition. When the condition is shifted from the DC voltage application condition to the normal operation, the frequency corresponding to the speed estimation value outputted from the speed estimation circuit 212 may be
20 set in the electric power converter 201, however, when the voltage command which is the induced voltage corresponding to the rotation speed of the AC motor is given and started, there is a possibility that the over current flows to the AC motor 202, and thereby, the smooth start can not be conducted. In
25 order to prevent this, the instantaneous power failure re-start control circuit 211 controls that the output voltage of the V/f converter 8 is gradually increased until it corresponds

to the normal induced voltage of the AC motor 202.

In the above examples, it is considered that only the exciting current control circuit 206 is operated, however, only the torque current control circuit 205 may be operated, or
5 neither current control circuits may also be operated.

Further, even when the exciting current command value id_{ref} is given and the current control is not conducted, when the DC voltage is applied, because the same phenomenon is generated, the speed estimation and rotation direction
10 detection become possible.

Further, when no residual voltage exists, the exciting current command value id_{ref} may be in one direction, however, when the residual voltage exists, by the amplitude and phase of the residual voltage, because the movement in the case of
15 the first time exciting current command value id_{ref} is changed, although the detection of the motor speed is possible, the rotation direction is detected in the case of the second time exciting current command value id_{ref} .

Further, when the motor speed is high, by also utilizing
20 the phenomenon that, in the case of the normal rotation, the exciting current detection value id_{fb} advances more than the torque current detection value i_{qfb} , and in the case of the reverse rotation, the exciting current detection value id_{fb} delays more than the torque current detection value i_{qfb} , the
25 rotation direction can be detected.

Further, the electric power conversion apparatus is described as the electric power conversion apparatus by which

the vector control is conducted in such a manner that the current flowing in the AC motor 2 is separated into the torque current and the exciting current, and respectively controlled independently, however, in also the electric power conversion apparatus by which the V/f constant control is conducted, when
5 the current control circuit by which the current flowing in the AC motor in the case of the instantaneous power failure, is separated into the torque current and the exciting current, and respectively controlled independently, is added, the
10 present invention can be conducted in the entirely same process. Further, in the above embodiment, it is described as the operation in the instantaneous power failure re-start time, however, even when the AC motor is started when it is in the free run condition for a long period of time, the present
15 invention can be conducted in the same processing as the above.

When conducted in this manner, also when the residual voltage exists in the AC motor or not, because the speed of the AC motor can be estimated, there is an advantage that the re-operation can be conducted quickly and smoothly at the
20 instantaneous power failure re-start time.

Industrial Possibility of Use

As described above, according to the present invention, when the AC motor is in the free run condition, the current
25 control is forcibly conducted so that the current of the AC motor is made zero, and on the base of the output voltage command signal to calculate by using the current control section output

in this case, because the phase and angular velocity of the residual voltage of the AC motor are obtained, there is an effect that the phase and angular velocity of the residual voltage can be accurately measured, and the re-operation can
5 be conducted quickly and smoothly at the instantaneous power failure re-start time. Further, when the phase and angular velocity of the residual voltage is obtained, because the previous speed signal is held in the holding circuit, and from the value to which the phase command signal is added, the phase
10 and angular velocity of the residual voltage are obtained, there is an effect that the continuity of the phase command signal is maintained, and the mechanical shock and the trip of the variable speed control apparatus are prevented, and the stable operation can be conducted.

[Claims]

1. A control method of an AC motor comprising:
an electric power converter to output an electric power
to an AC motor, and
5 a current control section to control the output current
of the electric power converter based on a difference signal
of an output current detection signal of a current command
signal and the electric power converter, wherein
when the AC motor is in the free run condition, the current
10 control is conducted by making the current command signal
forcibly zero so that the current of the AC motor is made zero;
and on the base of the output voltage command signal which is
calculated by using the current control section output, the
amplitude and phase and angular velocity of the residual
15 voltage of the AC motor are found.
2. A control method of the AC motor according to
Claim 1, wherein, when the amplitude and phase and angular
velocity of the residual voltage of the AC motor are found on
20 the base of the output voltage command signal, a signal holding
means is provided, and from the addition value of the phase
command signal just before the free run of the AC motor, and
the phase signal of the output voltage command signal, the
amplitude and phase and angular velocity of the residual
25 voltage are found.
3. A control method of the AC motor in which an

arbitrary electric power is outputted to the AC motor by the electric power converter; the current to be supplied to the motor is detected by a current detection circuit; the current control circuit controls so that the given current command
5 coincides with the current detection value detected by the current detection circuit; and the switching of the electric power converter is determined from the voltage command outputted from the current control circuit, the control method of the AC motor is characterized in that: a start control
10 circuit controls so that the electric power converter is normally operated at the start, and the speed of the AC motor in the free run condition is estimated by a speed estimation circuit.

15 4. A control method of the AC motor according to Claim 3, wherein the start control circuit forcibly makes the current command zero, and calculates the voltage command by which the current detection value is made zero, by the current control circuit, and by the time change of the voltage command, the
20 speed estimation circuit estimates the speed of the AC motor.

5. A control method of the AC motor according to Claim 3, wherein the start control circuit forcibly makes the current command zero, and calculates the voltage command by which the
25 current detection value is made zero, by the current control circuit, and when its voltage level is lower than the set voltage level, after the DC current command of set level is

applied for the set time period from zero, the current command is forcibly made zero again, by the current control circuit, the voltage command by which the current detection value is made zero, is calculated, and the speed estimation circuit
5 estimates the speed of the AC motor.

6. A control method of the AC motor according to any one of Claim 3, wherein the start control circuit forcibly makes the current command zero, and by the current control circuit,
10 the voltage command by which the current detection value is made zero, is calculated, and when its voltage level is lower than the set voltage level, after the DC current control command of the set level is applied for a set time period from zero, the current command is forcibly made zero again, and by the
15 current control circuit, even when the voltage command by which the current detection value is made zero, is calculated, when its voltage level is lower than the set voltage level, the speed estimation circuit estimates that the AC motor is stopped.

20 7. A control method of the AC motor according to any one of Claims 1 to 6, wherein the start control circuit forcibly makes the current command zero, and by the current control circuit, the voltage command by which the current detection value is made zero, is calculated, and by the time change of
25 the voltage command, the speed estimation circuit starts the AC motor by making the estimated speed of the AC motor and the amplitude and phase of the voltage command as the initial value.

8. A control method of the AC motor according to any one of Claims 1 to 6, wherein the start control circuit forcibly makes the current command zero, and by the current control
5 circuit, the voltage command by which the current detection value is made zero, is calculated, and by the time change of the voltage command, when the speed estimation circuit starts the AC motor by making the estimated speed of the AC motor and the amplitude and phase of the voltage command as the initial
10 value, the amplitude of the voltage command outputted from the electric power converter is gradually increased until it becomes the voltage level corresponding to the normal induced voltage to the speed of the AC motor.

15 9. A control apparatus of the AC motor, which has: an electric power converter to output an arbitrary electric power to the AC motor; current detection circuit to detect the current supplied to the motor; and current control circuit which controls so that the given current command coincides with
20 the current detection value detected by the current detection circuit, and in which the switching of the electric power converter is determined from the voltage command outputted from the current control circuit, the control apparatus of the AC motor is characterized in that it has the start control circuit,
25 and the speed estimation circuit to estimate the speed of the AC motor in the free run condition.

control circuit, even when the voltage command by which the current detection value is made zero, is calculated, when its voltage level is lower than the set voltage level, the speed estimation circuit estimates that the AC motor is stopped.

5

13. A control apparatus of the AC motor according to Claim 9, wherein the start control circuit forcibly makes the current command zero, and by the current control circuit, calculates the voltage command by which the current detection value is made zero, and by the time change of the voltage command, the speed estimation circuit starts the AC motor by making the estimated speed of the AC motor and the amplitude and phase of the voltage command as the initial value.

15 14. A control apparatus of the AC motor according to Claim 9, wherein the start control circuit forcibly makes the current command zero, and by the current control circuit, calculates the voltage command by which the current detection value is made zero, and by the time change of the voltage command, 20 when the speed estimation circuit starts the AC motor by making the estimated speed of the AC motor and the amplitude and phase of the voltage command as the initial value, the amplitude of the voltage command outputted from the electric power converter is gradually increased until it becomes the voltage level 25 corresponding to the normal induced voltage to the speed of the AC motor.

15. A control method of the AC motor according to Claim 3, wherein the start control circuit forcibly makes the current command zero, and by the current control circuit, calculates the voltage command by which the current detection value is made zero, and when the voltage command is larger than the set voltage level, by the time change of the phase of the voltage command, the speed estimation circuit estimates the speed of the AC motor, and as the initial value when the electric power converter is started, the amplitude and phase of the voltage command and the frequency corresponding to the speed estimation value of the AC motor are set, and it is started.

16. A control method of the AC motor which is characterized in that: it has an electric power converter to output the electric power to the AC motor, and the current control section by which the output current of the electric power converter is controlled, according to the difference signal of the current command signal and the output current detection signal of the electric power converter, in which, when the AC motor is in the free run condition, the arbitrary DC current is supplied to the AC motor for a set time period, and the frequency component appeared in the output current detection signal of the electric power converter is detected, and from this frequency component, the speed of the AC motor is estimated.

17. A control method of the AC motor according to Claim

3, wherein the start control circuit forcibly makes the current command zero, and by the current control circuit, the voltage command by which the current detection value is made zero, is calculated, and when its voltage level is lower than the set
5 voltage level, the DC current command of the set level or the DC voltage command of the set level is applied for a set time period from zero, and the speed estimation circuit detects the frequency component appeared in the current detection value, and estimates this frequency component as the speed of the AC
10 motor, and as the initial value when the electric power converter is started, the frequency corresponding to the speed estimation value of the AC motor is set, and it is started.

18. A control method of the AC motor according to Claim
15 3, wherein the start control circuit forcibly makes the current command zero, and by the current control circuit, the voltage command by which the current detection value is made zero, is calculated, and when the voltage command is lower than the set voltage level, the current command is changed from
20 zero to the DC current command value of the set level, and supplied for a set time period, and after that, the sign and the amplitude of the current command are changed, and applied for a set time period. The control method of the AC motor which is characterized in that, at this time, the speed estimation
25 circuit detects the frequency component appeared in the current detection value, and estimates this frequency component as the speed of the AC motor, and as the initial value when

the electric power converter is started, the frequency corresponding to the speed estimation value of the A motor is set, and it is started.

5 19. A control method of the AC motor according to Claim
3, wherein the start control circuit forcibly makes the
current command zero, and by the current control circuit, the
voltage command by which the current detection value is made
10 zero, is calculated, and when the voltage command is lower than
the set voltage level, the current control is stopped, and the
DC current command is applied for a set time period in the
arbitrary direction, after that, the arbitrary amplitude
current command is given in the direction in which the phase
is changed by 180° from the command direction of the DC voltage,
15 and the current control is conducted again for a set time period.
The control method of the AC motor which is characterized in
that, at this time, the speed estimation circuit detects the
frequency component appeared in the current detection value,
and estimates this frequency component as the speed of the AC
20 motor, and as the initial value when the electric power
converter is started, the frequency corresponding to the speed
estimation value of the AC motor is set, and it is started.

20. A control apparatus of the AC motor according to
25 Claim 9, wherein the start control circuit forcibly makes the
current command zero, and by the current control circuit, the
voltage command by which the current detection value is made

5

10

25

zero, is calculated, and when the voltage command is lower than the set voltage level, the current command is changed from zero to the DC current command value of the set level, and supplied for a set time period, and after that, the sign and the amplitude of the current command are changed, and applied for a set time period. The control apparatus of the AC motor which is characterized in that, at this time, the speed estimation circuit detects the frequency component appeared in the current detection value, and estimates this frequency component as the speed of the AC motor, and as the initial value when the electric power converter is started, the frequency corresponding to the speed estimation value of the A motor is set, and it is started.

23. A control apparatus of the AC motor according to Claim 9, wherein the start control circuit forcibly makes the current command zero, and by the current control circuit, the voltage command by which the current detection value is made zero, is calculated, and when the voltage command is lower than the set voltage level, the current control is stopped, and the DC voltage command is applied for a set time period in the arbitrary direction, after that, the arbitrary amplitude current command is given in the direction in which the phase is changed by 180° from the command direction of the DC voltage, and the current control is conducted again for a set time period. The control apparatus of the AC motor which is characterized in that, at this time, the speed estimation circuit detects the frequency component appeared in the current detection value,

and estimates this frequency component as the speed of the AC motor, and as the initial value when the electric power converter is started, the frequency corresponding to the speed estimation value of the AC motor is set, and it is started.

1. *Chlorophyll a* and *Chlorophyll b* content of the leaves was determined by the method of Arar and Johnson (1999). The leaves were ground in a mortar and pestle with 10 ml of 80% methanol. The extract was centrifuged at 10,000 rpm for 10 min. The supernatant was transferred to a test tube and the residue was re-extracted with 5 ml of 80% methanol. The extracts were combined and the solvent was evaporated under reduced pressure. The residue was dissolved in 10 ml of 80% methanol. The absorbance of the extract was measured at 663 nm and 646 nm. The concentration of chlorophyll *a* and *b* was calculated using the following equations:

1. *Chlorophyll a* and *Chlorophyll b* content of the leaves was determined by the method of Arar and Johnson (1999). The leaves were ground in a mortar and pestle with 10 ml of 80% methanol. The extract was centrifuged at 10,000 rpm for 10 min. The supernatant was transferred to a test tube and the residue was re-extracted with 5 ml of 80% methanol. The extracts were combined and the solvent was evaporated under reduced pressure. The residue was dissolved in 10 ml of 80% methanol. The absorbance of the extract was measured at 663 nm and 646 nm. The concentration of chlorophyll *a* and *b* was calculated using the following equations:

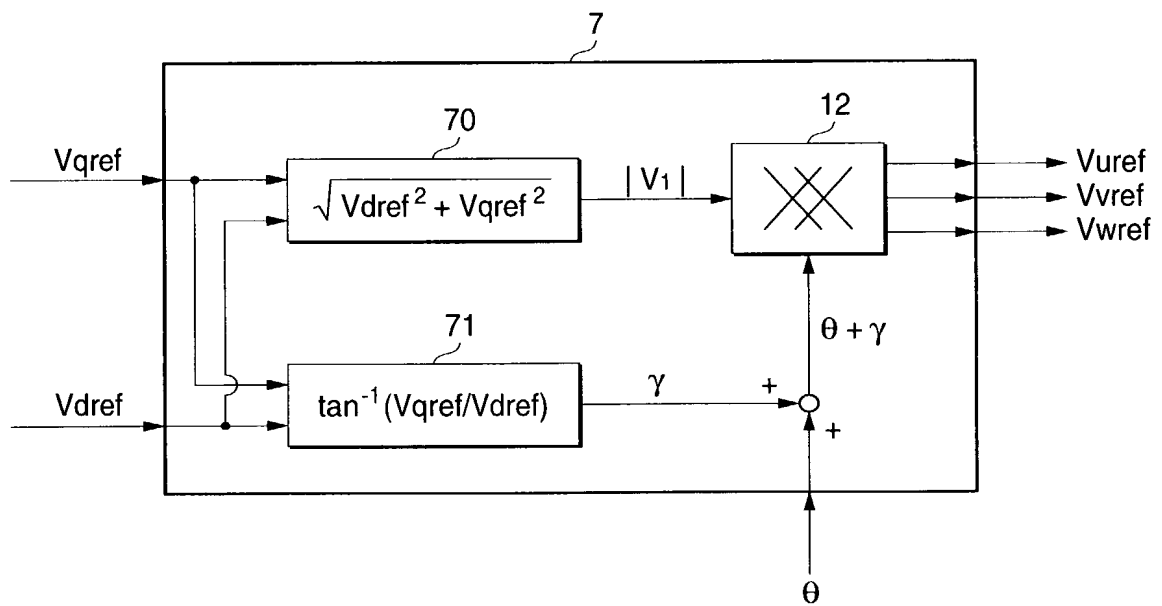
1. *Chlorophyll a* and *Chlorophyll b* content of the leaves was determined by the method of Arar and Johnson (1999). The leaves were ground in a mortar and pestle with 10 ml of 80% methanol. The extract was centrifuged at 10,000 rpm for 10 min. The supernatant was transferred to a test tube and the residue was re-extracted with 5 ml of 80% methanol. The extracts were combined and the solvent was evaporated under reduced pressure. The residue was dissolved in 10 ml of 80% methanol. The absorbance of the extract was measured at 663 nm and 646 nm. The concentration of chlorophyll *a* and *b* was calculated using the following equations:

FIG. 1



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FIG. 2



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FIG. 3

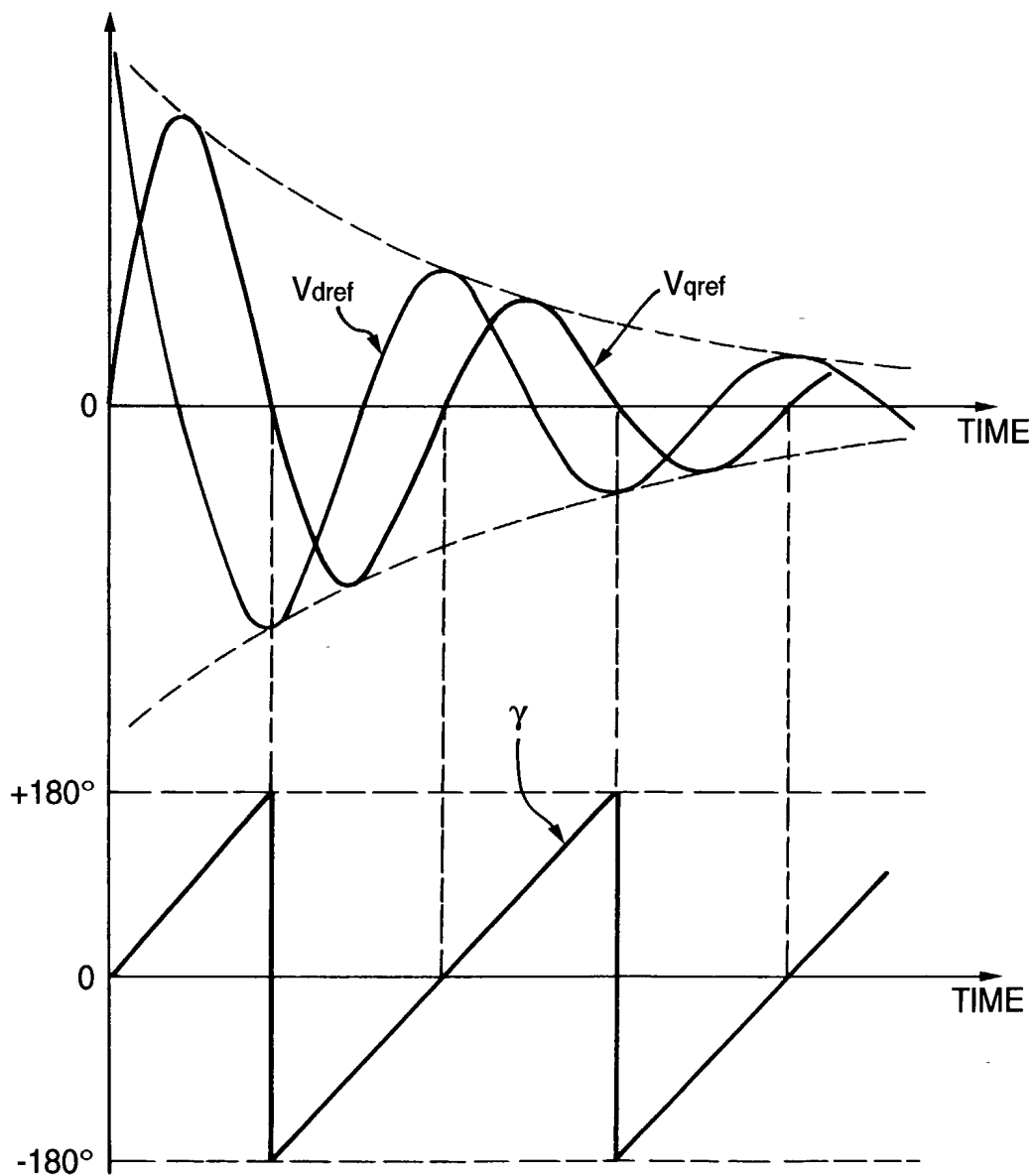


FIG. 5

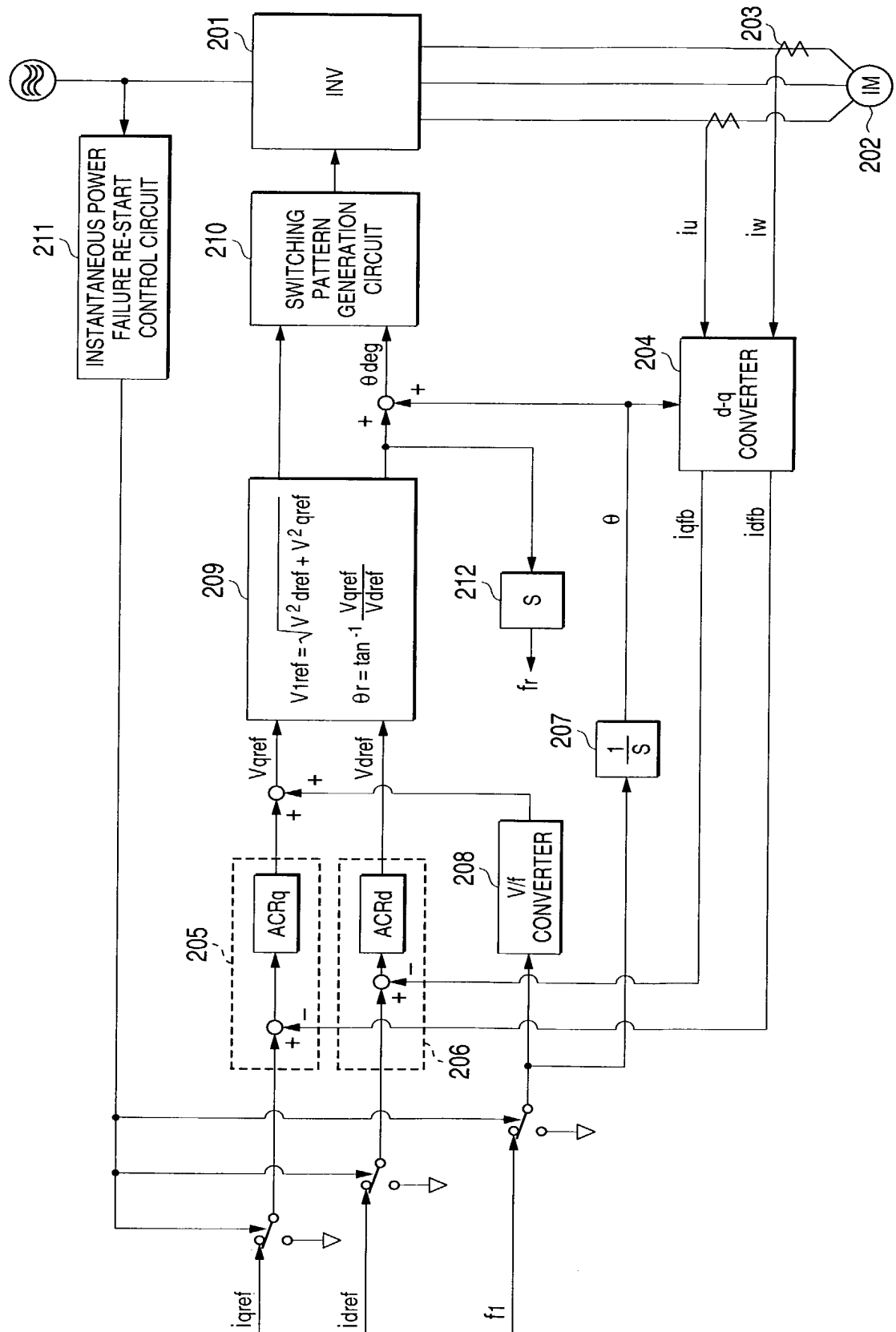


FIG. 6 (b)

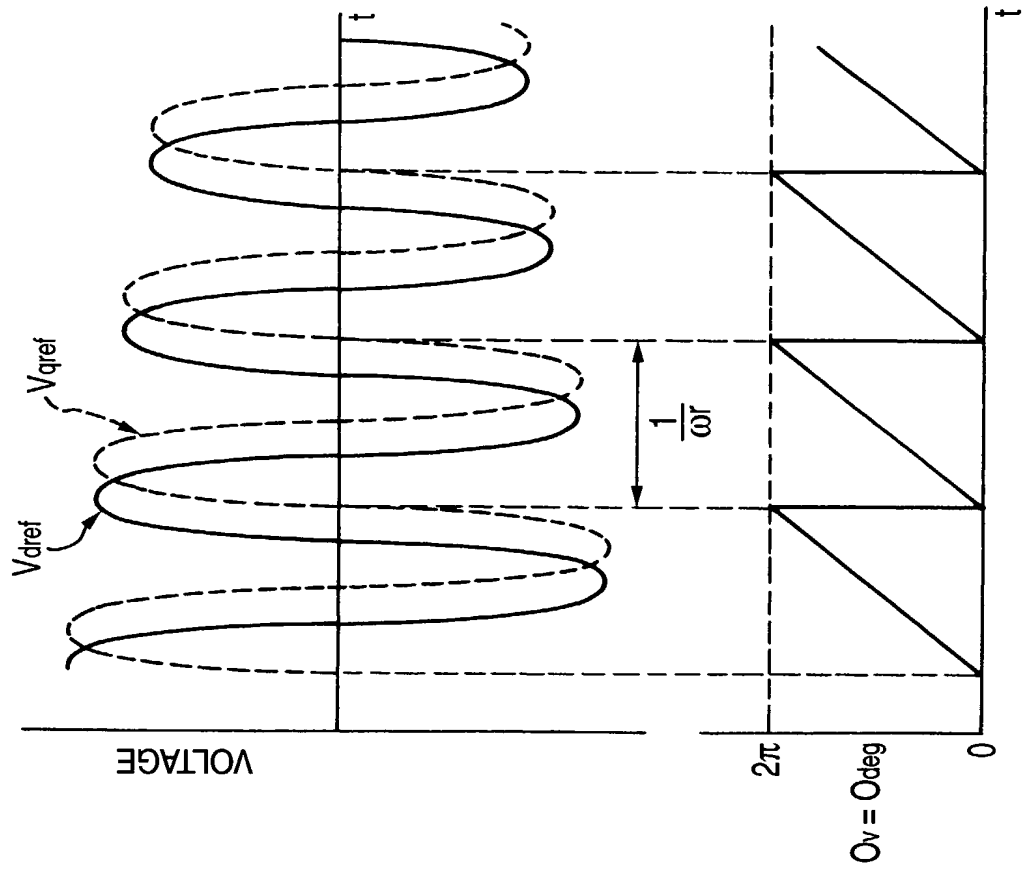


FIG. 6 (a)

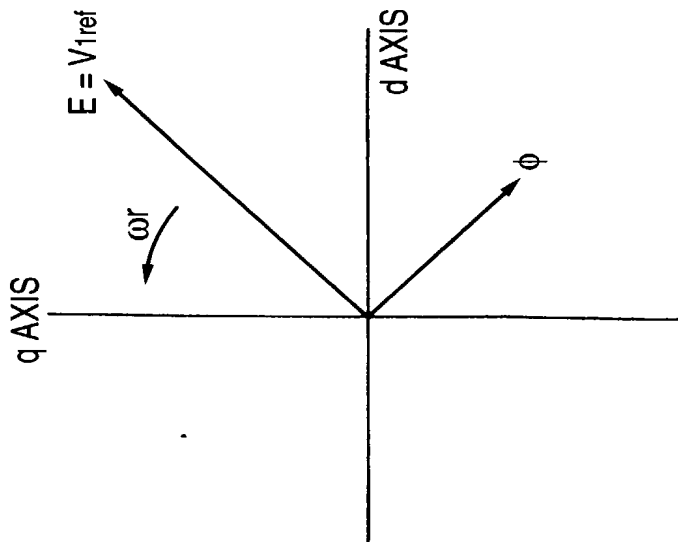


FIG. 7 (a)

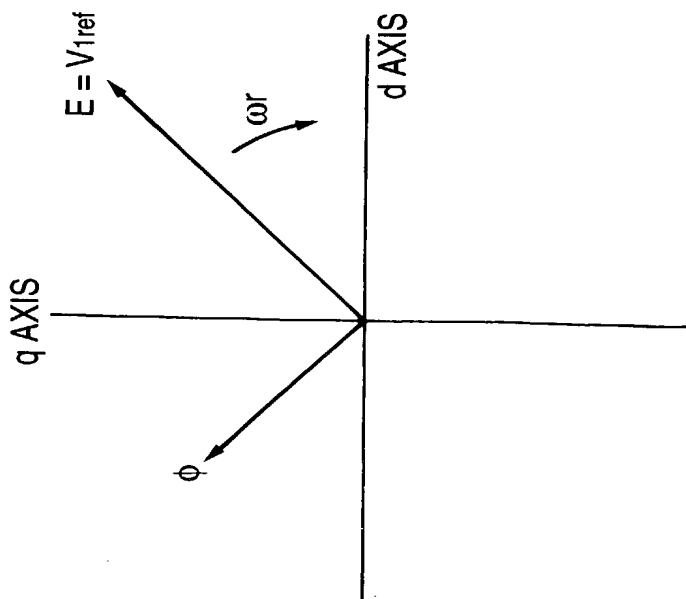
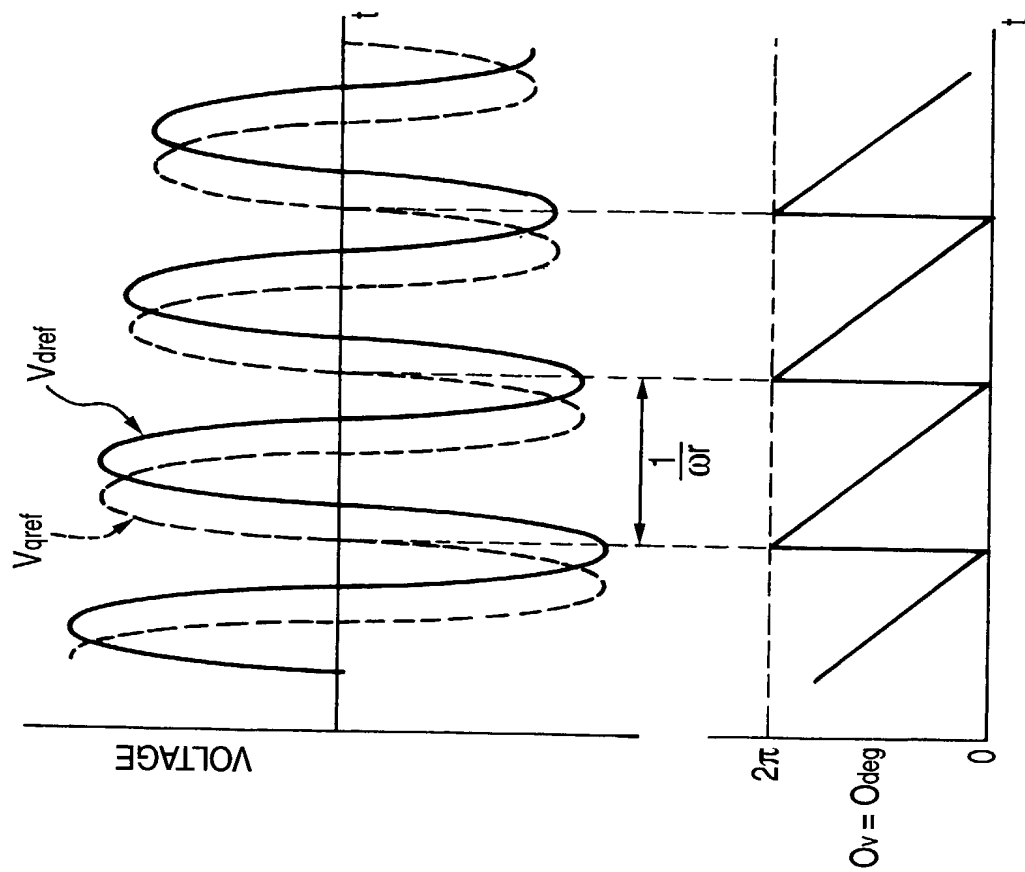


FIG. 7 (b)



[illegible]

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FIG. 9 (a)

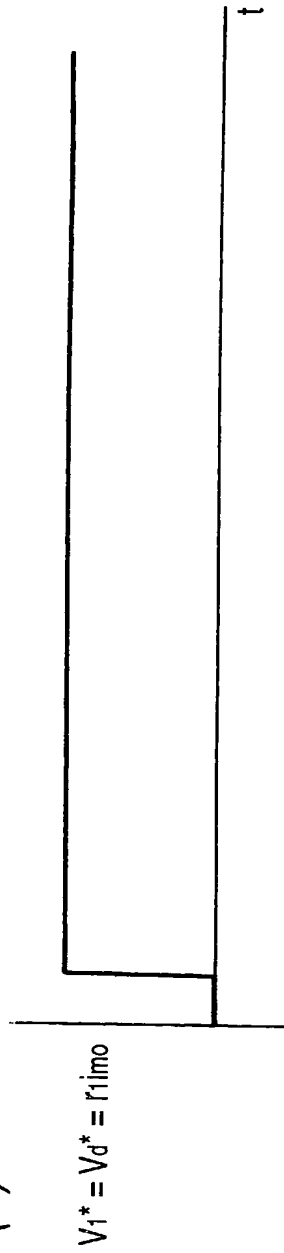


FIG. 9 (b)

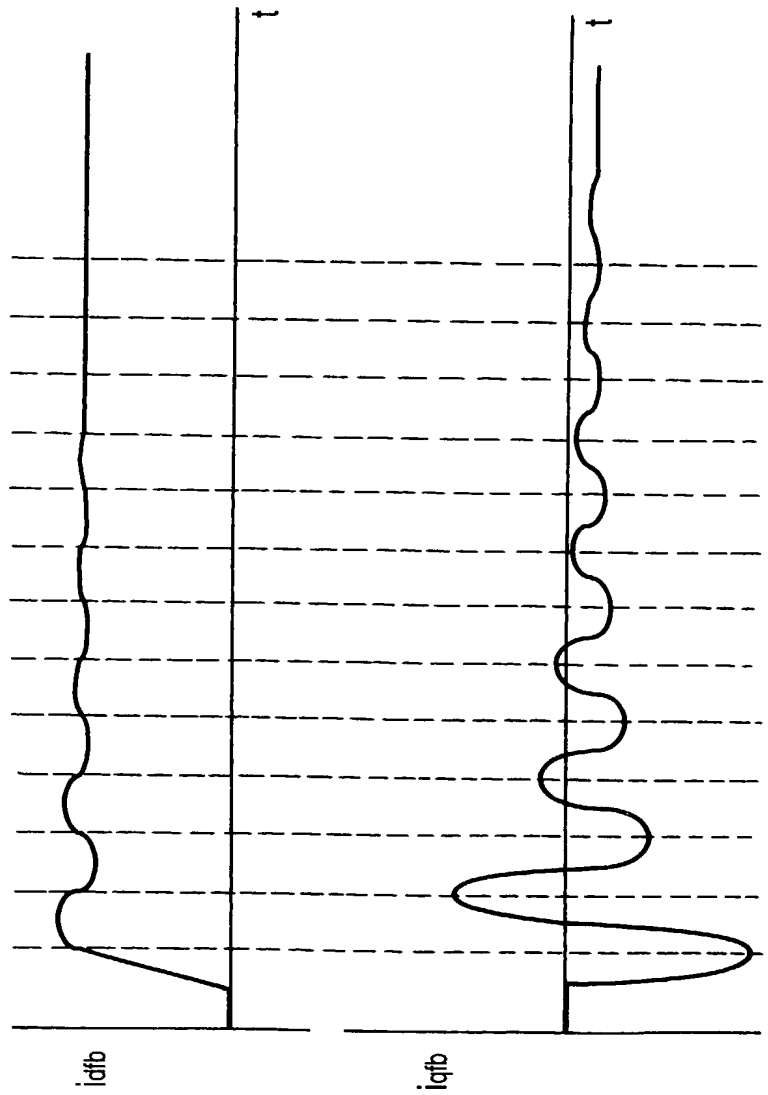
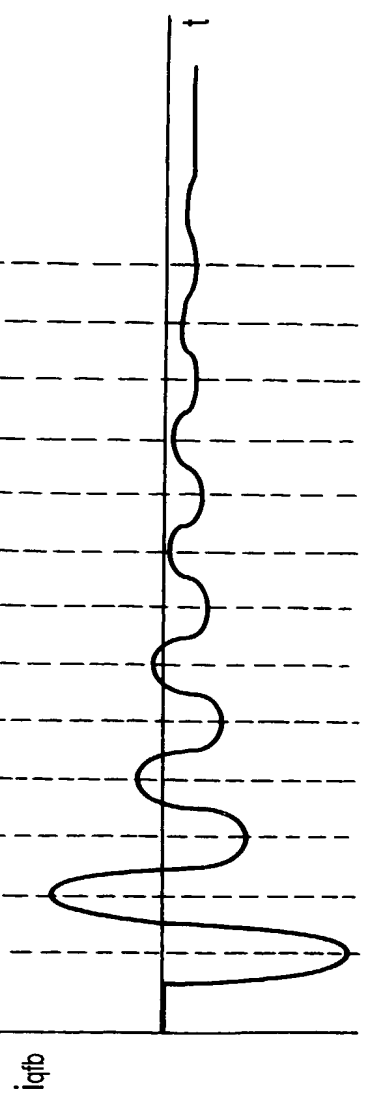


FIG. 9 (c)



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FIG. 10 (a)

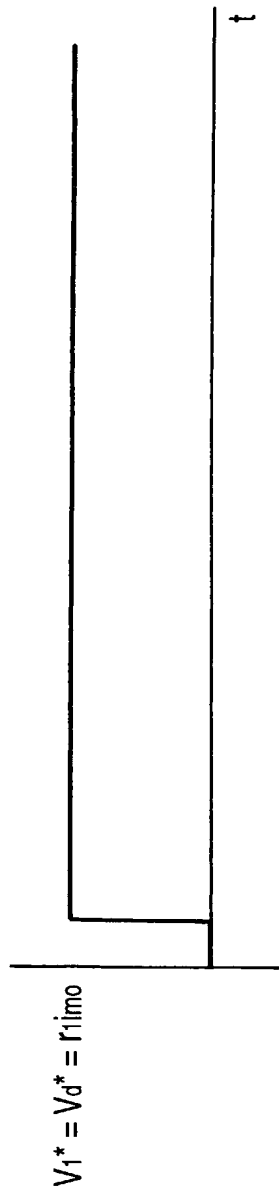


FIG. 10 (b)

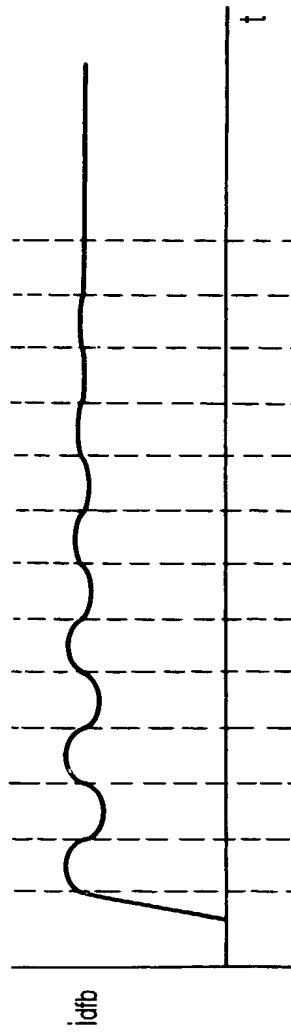


FIG. 10 (c)

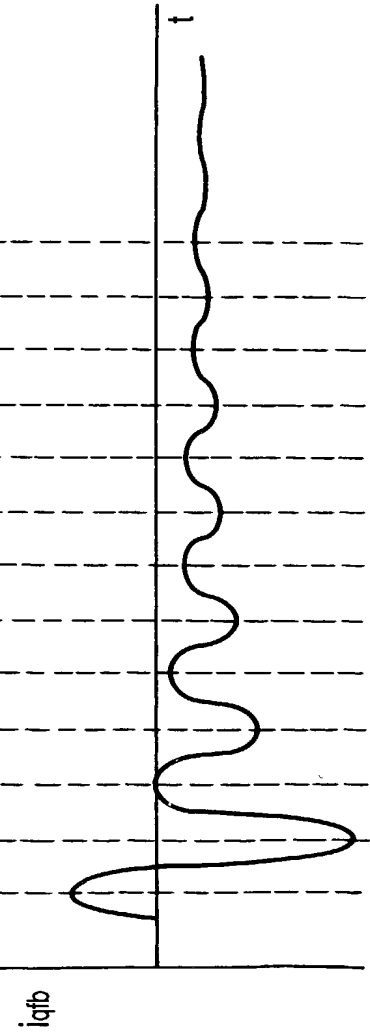
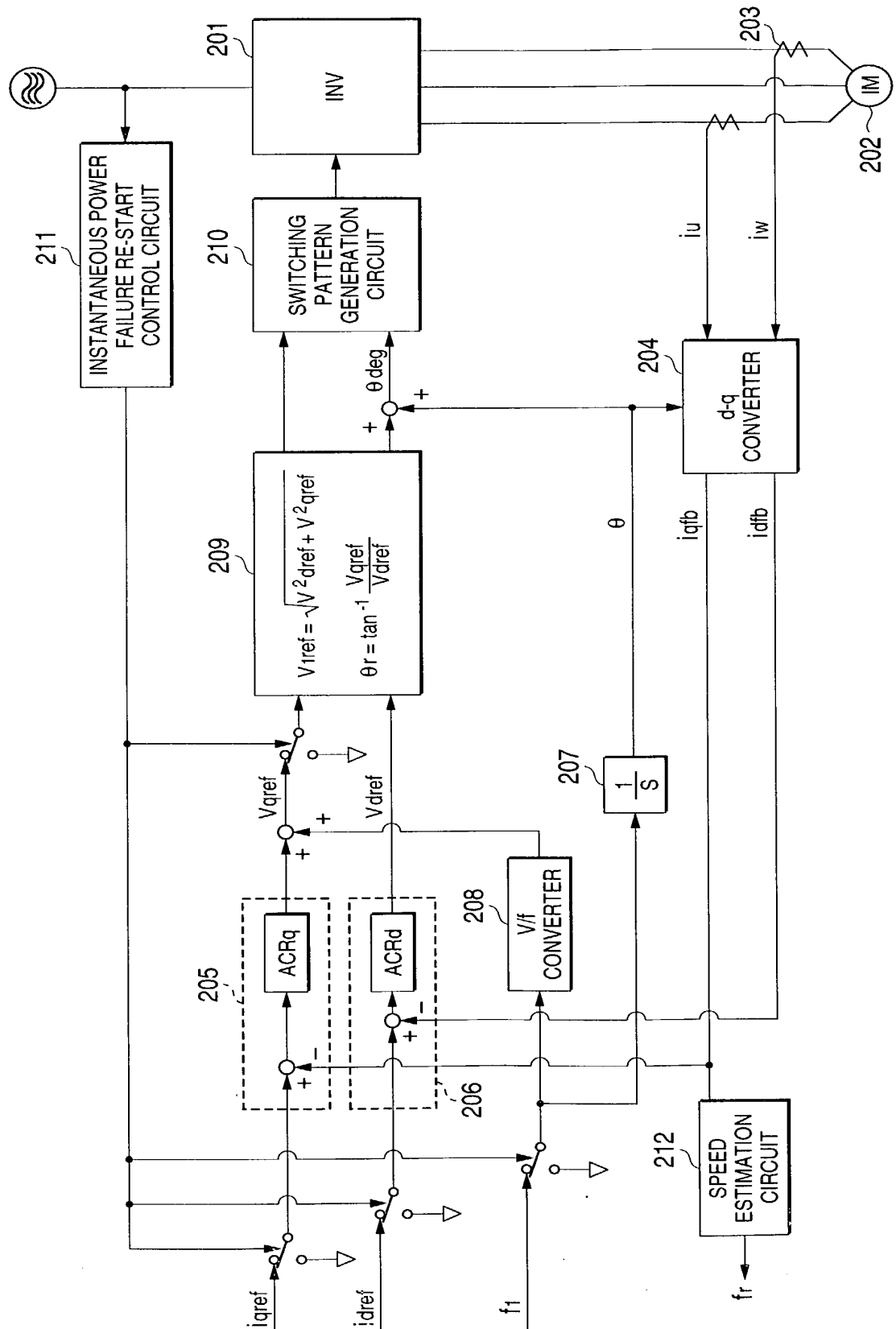


FIG. 11



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FIG. 12

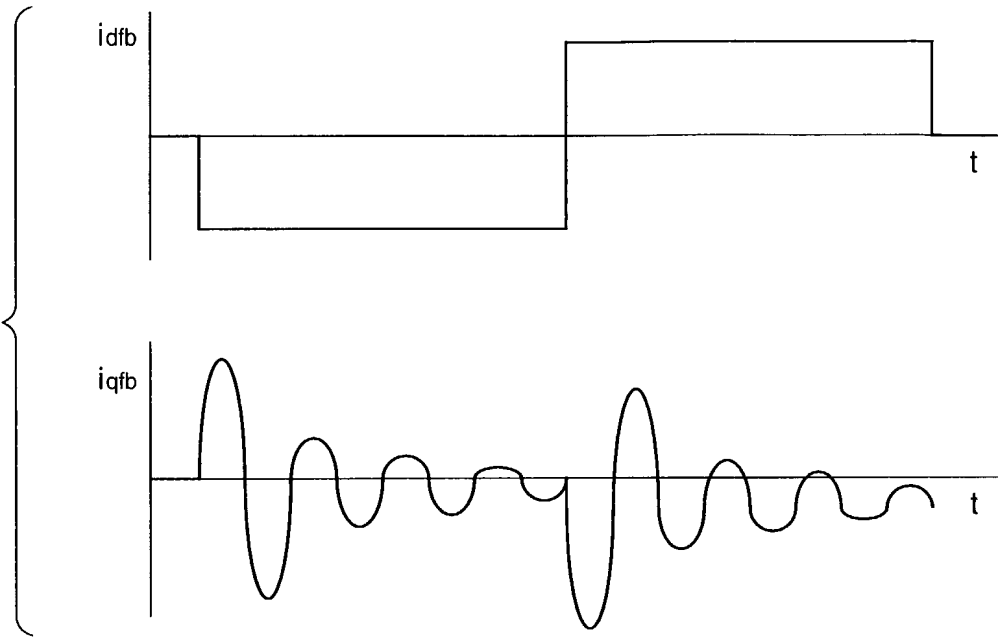
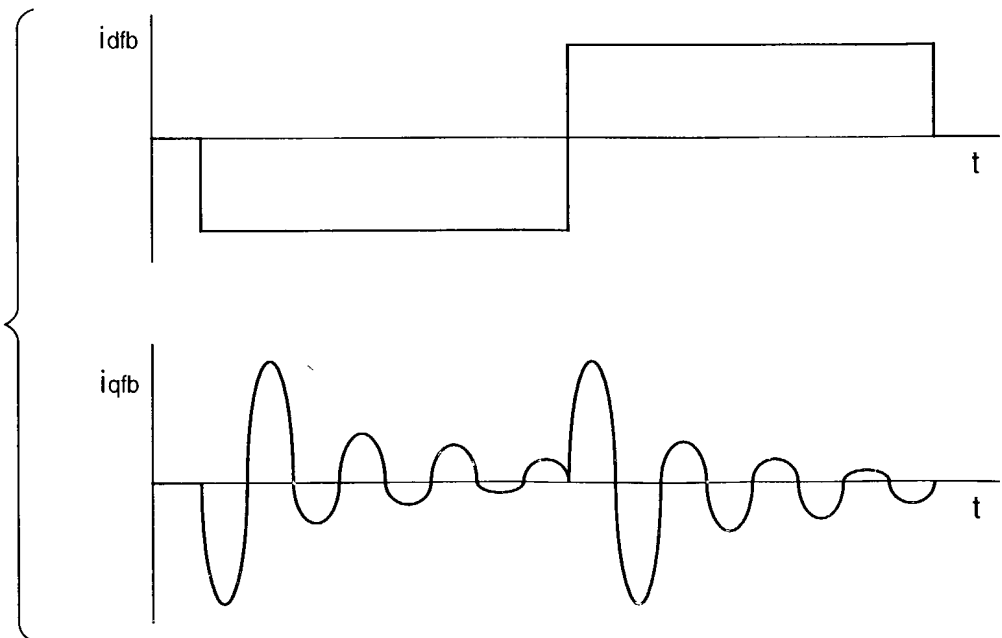


FIG. 13



Declaration and Power of Attorney for Patent Application 特許出願宣言書および委任状

Japanese Language Declaration

日本語宣言書

私は下記発明者として以下の通り宣言します：

As a below named inventor, I hereby declare that:

私の住所、郵送先、および国籍は私の氏名の後に記載された通りです。

My residence, mailing address and citizenship are as stated next to my name.

下記名称の発明に関し請求範囲に記載され特許出願がされている発明内容につき、私が最初、最先かつ唯一の発明者（下記氏名が一つのみの場合）であるか、あるいは最初、最先かつ共同発明者（下記氏名が複数の場合）であると思います。

I believe I am the original, first and sole inventor (if only one name is listed below) or an original, first and joint inventor (if plural names are listed below) of the subject matter which is claimed and for which a patent is sought on the invention entitled

CONTROL METHOD OF AC MOTOR AND
CONTROL APPARATUS THEREOF

下記項目にx印が付いている場合を除き、上記発明の明細書は本書に添付されます。

the specification of which is attached hereto unless the following box is checked:

☐ 上記発明は米国出願番号あるいはPCT国際出願番号（確認番号_____）として_____年__月__日に出願され、
_____年__月__日に補正されました（該当する場合）。

☒ was filed on September 13, 2000
as United States Application Number or
PCT International Application Number
PTC/JP00/06271 (Conf. No. _____)
and was amended on _____
(if applicable).

私は特許請求範囲を含み上述の補正で補正された前記明細書の内容を検討し、理解していることをここに表明します。

I hereby state that I have reviewed and understand the contents of the above identified specification, including the claims, as amended by any amendment referred to above.

私は連邦規則法典第 37 編 1 条 56 項に定義される特許性に肝要な情報について開示義務があることを認めます。

I acknowledge the duty to disclose information which is material to patentability as defined in Title 37, Code of Federal Regulations, § 1.56.

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私は米国法典第 35 編 119 条(a)-(d)あるいは 365 条(b)に基づき特許あるいは発明者証書の下記外国出願、または 365 条(a)に基づき米国以外の少なくとも 1 ヶ国を指定した下記 PCT 外国出願についての外国優先権をここに主張するとともに、下記項目に×印を付けることにより優先権を主張する出願以前の出願日を有する特許あるいは発明者証書の外国出願あるいは PCT 外国出願を示します。

Prior foreign application(s)

外国での先行出願

Priority Claimed

優先権の主張

Yes No
有り 無し

P.Hei. 11-267499

Japan

21/September/1999

(Number)

(Country)

(Day/Month/Year Filed)

(番号)

(国名)

(出願年月日)

☒☐

P2000-231526

Japan

31/July/2000

(Number)

(Country)

(Day/Month/Year Filed)

(番号)

(国名)

(出願年月日)

☒☐

私は米国法典第 35 編 119 条(e)に基づき下記の米国仮特許の利益をここに主張します。

I hereby claim the benefit under Title 35, United States Code, § 119(e) of any United States provisional application(s) listed below

(Application No.)
(出願番号)(Filing Date)
(出願日)(Application No.)
(出願番号)(Filing Date)
(出願日)

私は米国法典第 35 編 120 条に基づき下記米国特許出願、あるいは 365 条(c)に基づき米国を指定する下記 PCT 国際特許出願の利益をここに主張し、本特許出願内特許請求範囲の各項目の内容が米国法典第 35 編 112 条の最初の項に規定される方法により先行米国あるいは PCT 国際特許出願で開示されていない限りにおいて連邦規則法典第 37 編 1 条 56 項に定義される特許性に肝要で、先行特許出願の出願日から本特許出願の国内あるいは PCT の出願日までの間に入手された情報について開示義務があることを認めます。

I hereby claim the benefit under Title 35, United States Code, § 120 of any United States application(s), or § 365(c) of any PCT International application designating the United States, listed below and, insofar as the subject matter of each of the claims of this application is not disclosed in the prior United States or PCT International application in the manner provided by the first paragraph of Title 35, United States Code, § 112, I acknowledge the duty to disclose information which is material to patentability as defined in Title 37, Code of Federal Regulations, § 1.56 which became available between the filing date of the prior application and the national or PCT International filing date of this application.

(Application No.)
(出願番号)(Filing Date)
(出願日)(Status: patented, pending, abandoned)
(状態: 特許成立済、係属中、放棄済)(Application No.)
(出願番号)(Filing Date)
(出願日)(Status: patented, pending, abandoned)
(状態: 特許成立済、係属中、放棄済)

私は本宣言書内で私自身の知識に基づいてなされたすべての陳述が真実であり、情報および信ずるところに基づいてなされたすべての陳述が真実であると信じられていることをここに宣言し、さらに故意になされた虚偽の陳述等々は米国法典第 18 編 1001 条に基づき罰金あるいは拘禁または両方による処罰にあたり、またかような故意による虚偽の陳述はそれに基づく特許出願あるいは成立特許の有効性を危うくする可能性があることを認識した上でこれらの陳述をなしたことを宣言します。

I hereby declare that all statements made herein of my own knowledge are true and that all statements made on information and belief are believed to be true; and further that these statements were made with the knowledge that willful false statements and the like so made are punishable by fine or imprisonment, or both, under Section 1001 of Title 18 of the United States Code and that such willful false statements may jeopardize the validity of the application or any patent issued thereon.

Japanese Language Declaration

日本語宣言書

委任状：私は下記の米国特許商標局（USPTO）顧客番号のもとに記載される SUGHRUE MION 法律事務所のすべての弁護士を、同顧客番号のもとに記載される個々の弁護士は SUGHRUE MION 法律事務所のみ自由裁量に基づき変更され得ることを認識した上で、本特許出願の手続きおよびそれに関わる特許商標局との業務を遂行する弁護士として指名し、本特許出願に関するすべての通信が同 USPTO 顧客番号のもとに提出された住所宛に送付されることを要請します。

POWER OF ATTORNEY: I hereby appoint all attorneys of SUGHRUE MION, PLLC who are listed under the USPTO Customer Number shown below as my attorneys to prosecute this application and to transact all business in the Patent and Trademark Office connected therewith, recognizing that the specific attorneys listed under that Customer Number may be changed from time to time at the sole discretion of SUGHRUE MION, PLLC, and request that all correspondence about the application be addressed to the address filed under the same USPTO Customer Number.



23373

PATENT TRADEMARK OFFICE

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300

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Citizenship 国籍		Japan	
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Fourth inventor's signature 第四発明者の署名		Date 日付	
Residence 住所			
Citizenship 国籍			
Mailing Address 郵送先			
Full name of fifth joint inventor, if any 第五の共同発明者名(該当する場合)			
Fifth inventor's signature 第五発明者の署名		Date 日付	
Residence 住所			
Citizenship 国籍			
Mailing Address 郵送先			
Full name of sixth joint inventor, if any 第六の共同発明者名(該当する場合)			
Sixth inventor's signature 第六発明者の署名		Date 日付	
Residence 住所			
Citizenship 国籍			
Mailing Address 郵送先			